

Mysteries of the Smith Chart

*Transmission Lines, Impedance Matching,
and Little Known Facts*

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□ ***Transmission Line Theory***

- Historical development
- Heaviside's rewrite of Maxwell's theory, Telegrapher's equations,
- Impedance, reflection coefficient, SWR, phase constant, & velocity factor
- Special facts for $\lambda/2$, $\lambda/4$, and $\lambda/8$ lossless lines

□ ***The Smith Chart***

- Bilinear complex functions
- Impedance and admittance coordinates (circles, circles, and more circles)

□ ***Impedance Matching***

- Why match? Impedance matching vs. conjugate impedance matching
- Single frequency matching
- Multiple-frequency and broadband matching

Part 1: Transmission Line Theory

- 1830's magnetic telegraphs - Gauss, Henry***
- 1839 electromagnetic telegraph - Wheatstone & Cook***
- 1844 telegraph in America - Morse***
- 1850's thousands of miles of telegraph line U.S. and Europe***
- 1851 40 mile cable under English Channel***
- 1855 distributed analysis of transmission line - Lord Kelvin***
- 1858 transatlantic cable, project delayed by civil war***
- 1873 theory of electrodynamics - Maxwell***
- 1876 invention of telephone - Bell***
- 1880's vectors, vector calculus, reformulation of Maxwell's theory, transmission line theory - Heaviside***
- 1886 experimental confirmation of Maxwell's Theory - Hertz***
- 1937 early Smith Chart, published 1939 & 1944 - Smith***

$$\nabla \times \mathbf{E} = -\frac{\partial \mathbf{B}}{\partial t}$$

$$\nabla \times \mathbf{H} = \mathbf{J} + \frac{\partial \mathbf{D}}{\partial t}$$

$$\nabla \cdot \mathbf{D} = \rho$$

$$\nabla \cdot \mathbf{B} = 0$$

$$\mathbf{D} = \epsilon \mathbf{E}$$

$$\mathbf{B} = \mu \mathbf{H}$$

“And God said, Let there be light; and there was light.” Genesis 1:3

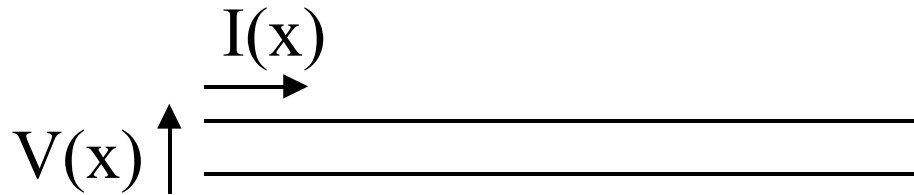
$$\nabla \times \mathbf{E} = -j\omega\mu\mathbf{H}$$

$$\nabla \times \mathbf{H} = (\sigma + j\omega\epsilon)\mathbf{E}$$

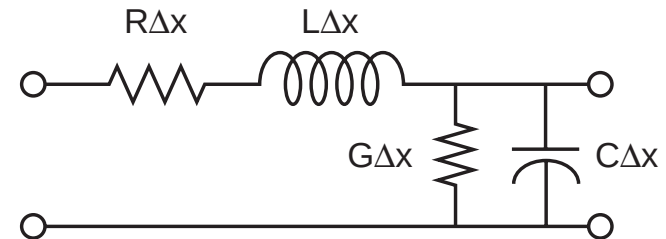
$$\nabla \cdot \mathbf{E} = 0$$

$$\nabla \cdot \mathbf{H} = 0$$

Uniform transmission line



Equivalent circuit of infinitesimal segment



$$\frac{dV}{dx} = -(R + j\omega L)I(x)$$

$$\frac{dI}{dx} = -(G + j\omega C)V(x)$$

Transmission Line Solution

TEM Waves

Traveling wave

$$V(x) = V_o e^{j\gamma x}$$

$$I(x) = \frac{V(x)}{Z_o}$$

Propagation constant

$$\gamma = \alpha + j\beta = \sqrt{(R + j\omega L)(G + j\omega C)}$$

Characteristic impedance

$$Z_o = \sqrt{\frac{R + j\omega L}{G + j\omega C}}$$

Real Parameters

R = series resistance per unit length (Ohms/meter)

L = series inductance per unit length (Henries/meter)

G = shunt conductance per unit length (Siemens/meter)

C = shunt capacitance per unit length (Farads/meter)

α = attenuation constant (nepers/meter)

β = phase constant (radians/meter)

λ = wavelength (meters)

v_f = velocity factor (dimensionless)

X = reactance (Ohms)

B = susceptance (Siemens)

s = standing wave ratio (dimensionless)

Notations (Cont'd)

Complex Parameters



$Z = R + jX = \text{impedance (Ohms)}$

$Z_L = \text{load impedance (Ohms)}$

$Z_i = \text{input impedance (Ohms)}$

$Z_0 = \text{characteristic impedance (Ohms)}$

$z = Z/Z_0 = r + jx = \text{normalized impedance (dimensionless)}$

$Y = G + jB = \text{admittance (Siemens)}$

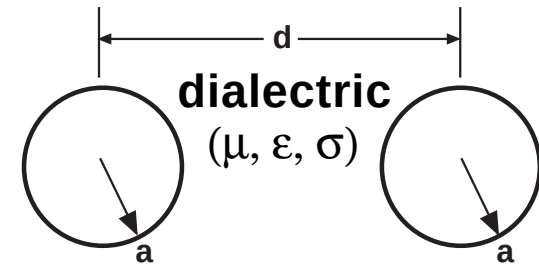
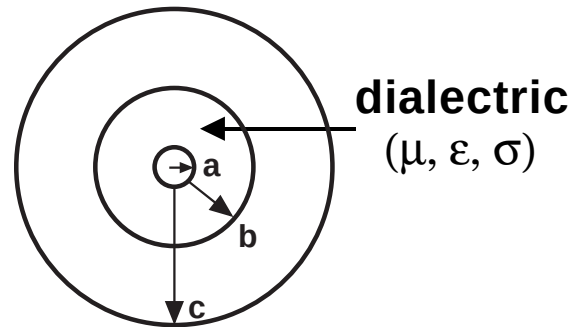
$y = Y/Y_0 = g + jb = \text{normalized admittance (dimensionless)}$

$\Gamma = \Gamma_r + j \Gamma_i = \text{complex reflection coefficient (dimensionless)}$

$\gamma = \alpha + j\beta = \text{propagation constant (inverse meters)}$

Transmission Line Parameters

Physical Dimensions and Material Properties



Parameter

Coax

Twinlead

R Ω/m

$$\frac{1}{2\pi\delta\sigma_c} \left(\frac{1}{a} + \frac{1}{b} \right)$$

$$\frac{1}{\pi a \delta \sigma_c}$$

L H/m

$$\frac{\mu}{2\pi} \left[\ln \frac{b}{a} + \frac{\delta}{2} \left(\frac{1}{a} + \frac{1}{b} \right) \right]$$

$$\frac{\mu}{\pi} \left[\frac{\delta}{2a} + \cosh^{-1} \frac{d}{2a} \right]$$

G S/m

$$\frac{2\pi\sigma}{\ln \frac{b}{a}}$$

$$\frac{\pi\sigma}{\cosh^{-1} \frac{d}{2a}}$$

C F/m

$$\frac{2\pi\epsilon}{\ln \frac{b}{a}}$$

$$\frac{\pi\epsilon}{\cosh^{-1} \frac{d}{2a}}$$

where skin depth is

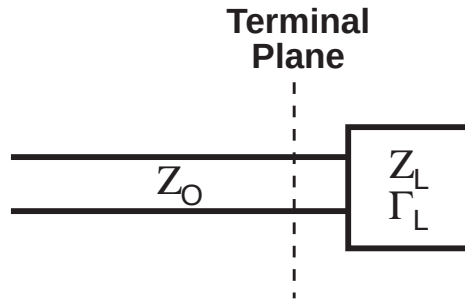
$$\delta = \frac{1}{\sqrt{\pi f \mu \sigma_c}}$$

for copper

$$\sigma_c = 5.8 \times 10^7 \text{ S/m}$$

$$\delta = \begin{cases} 8.5 \text{ mm at 60 Hz} \\ 6.6 \mu\text{m at 100 MHz} \end{cases}$$

Reflection Coefficient and Impedance Relation at a Terminal Plane



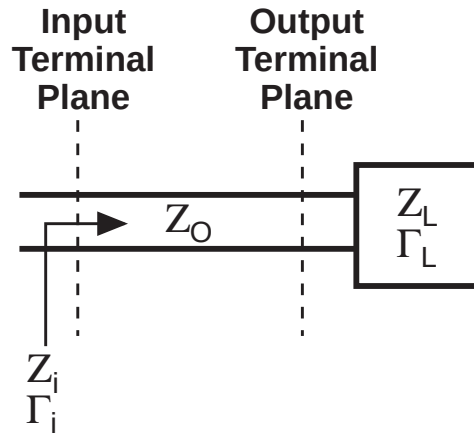
Definition

$$\Gamma = \frac{Z_L - Z_o}{Z_L + Z_o} = \frac{z - 1}{z + 1}$$

Inverse

$$z = \frac{1 + \Gamma}{1 - \Gamma}$$

- For every terminal plane, the complex load impedance and complex reflection coefficient seen to the right give the same information for that terminal plane***
- Question: How do Γ and z change as the terminal plane moves?***



Impedance relation

$$Z_i = \frac{Z_L + j \tan \beta l}{1 + j Z_L \tan \beta l}$$

Cross relations

$$Z_i = \frac{1 + \Gamma_L e^{-j2\beta l}}{1 - \Gamma_L e^{-j2\beta l}}$$

$$Z_L = \frac{1 + \Gamma_i e^{j2\beta l}}{1 - \Gamma_i e^{j2\beta l}}$$

Reflection coefficient relation

$$\Gamma_i = \Gamma_L e^{-j2\beta l}$$

Wavelength

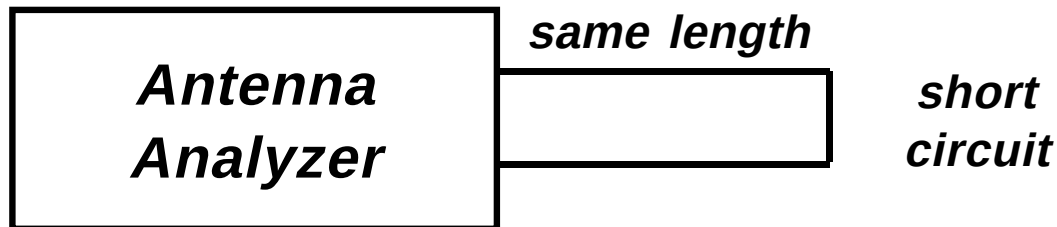
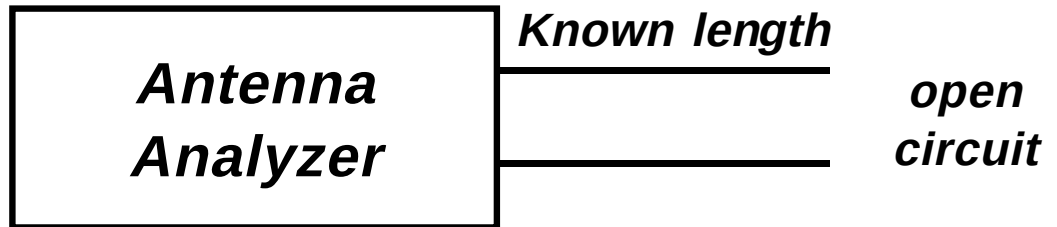
$$\lambda_{\text{free space}} = \frac{c}{f}$$

$$\lambda_{\text{actual}} = \frac{v}{f}$$

Velocity factor

$$v_f = \frac{v}{c} = \frac{\lambda_{\text{actual}}}{\lambda_{\text{free space}}}$$

How To Measure Velocity Factor of a Line (One Way To Do It)



$$v_f = \frac{2\pi fl}{c} \frac{1}{\cot^{-1} \sqrt{\frac{-Z_{open}}{Z_{short}}}}$$

$$\beta = \frac{2\pi}{\lambda_{\text{actual}}} = \frac{2\pi f}{v_f c} \quad \text{radians/meter}$$

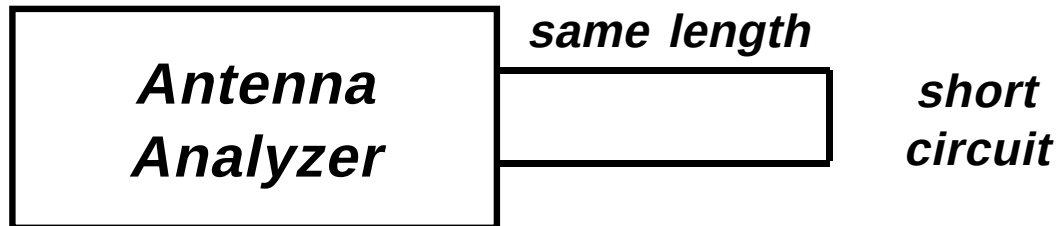
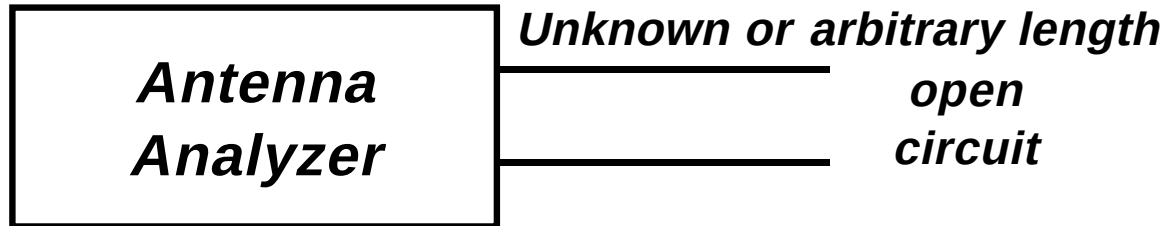
- ❑ ***Phase constant β and velocity factor v_f give equivalent information***
- ❑ ***Both can be calculated from line dimensions and material properties***

$$\beta = \text{Im} \sqrt{(R + j\omega L)(G + j\omega C)}$$

- ❑ ***Best to measure!***

How to Measure Complex Z_o of A Line

(One Way to Do It)



$$Z_o = \sqrt{Z_{open} \times Z_{short}}$$

- ❑ ***Geometric mean of two complex numbers***
- ❑ ***Calculation is trivial in polar form on Smith Chart***

Half wavelength, $l = \lambda/2$

$$Z_i = Z_L$$

Quarter wavelength, $l = \lambda/4$

$$Z_i = \frac{Z_o^2}{Z_L}$$

Eighth wavelength, $l = \lambda/8$

$$|Z_i| = Z_o \quad \text{if } Z_L \text{ and } Z_o \text{ are real (resistive)}$$

Easy to remember from

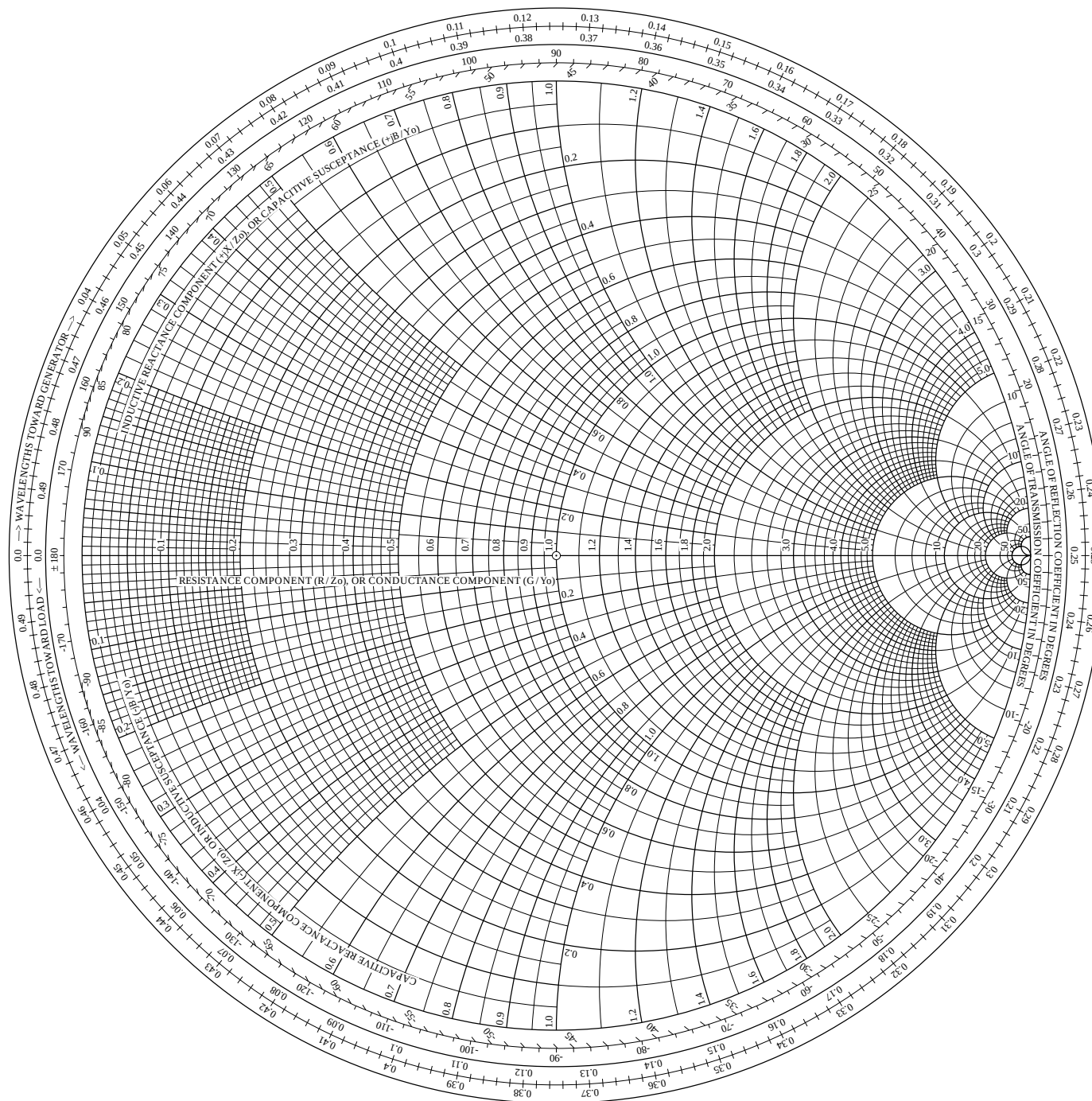
$$s = \frac{1 + |\Gamma|}{1 - |\Gamma|}$$

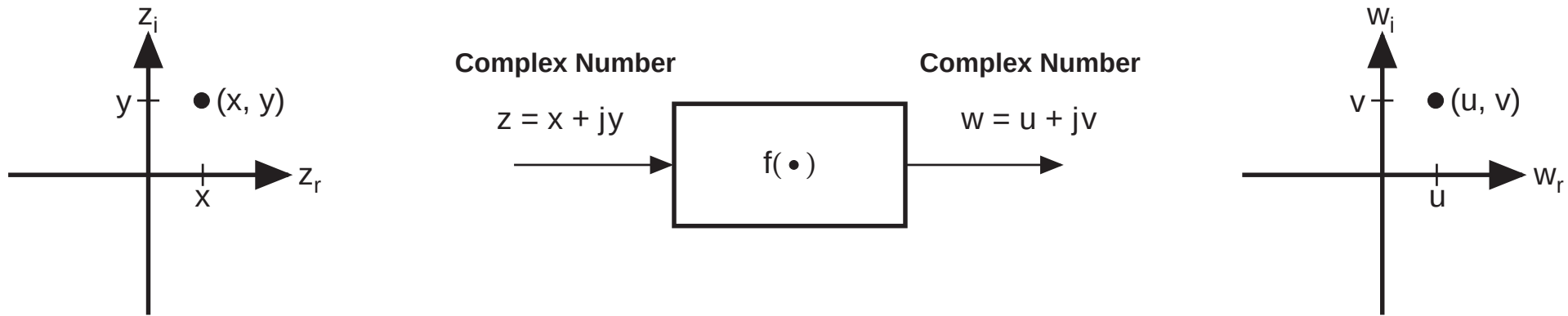
$$|\Gamma| = \frac{s - 1}{s + 1}$$

$$z = \frac{1 + \Gamma}{1 - \Gamma}$$

$$\Gamma = \frac{z - 1}{z + 1}$$

Part 2: The Smith Chart





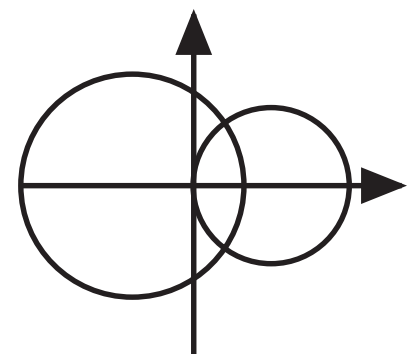
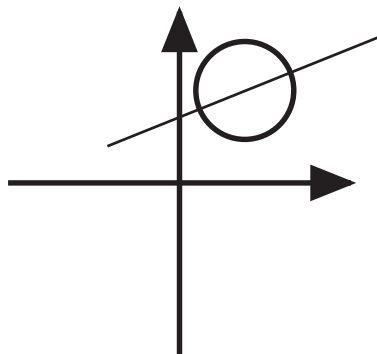
□ *Basic types of complex functions*

➤ Global Properties

- Linear – lines map to lines
- Bilinear – circles map to circles

➤ Local Properties

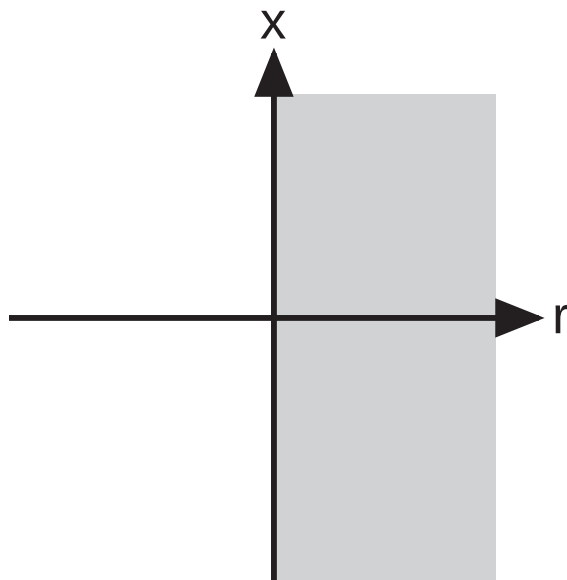
- Conformal – right angles map to right angles



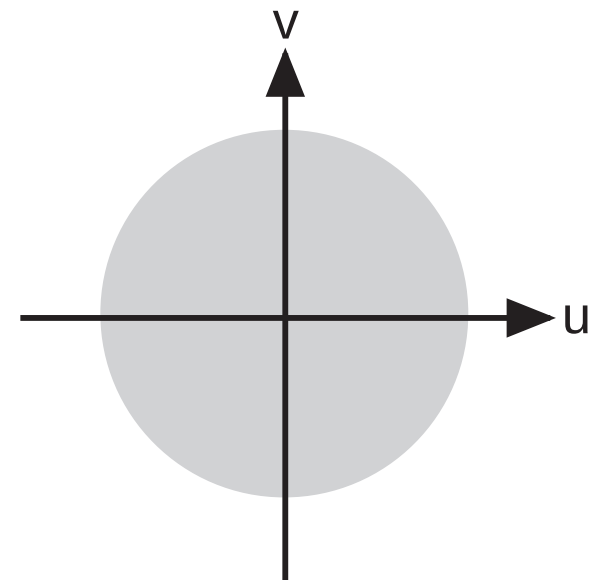
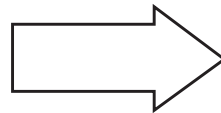
$$\Gamma = \frac{z - 1}{z + 1}$$

*a bilinear conformal
complex function*

$$u + jv = \frac{(r - 1) + jx}{(r + 1) + jx}$$



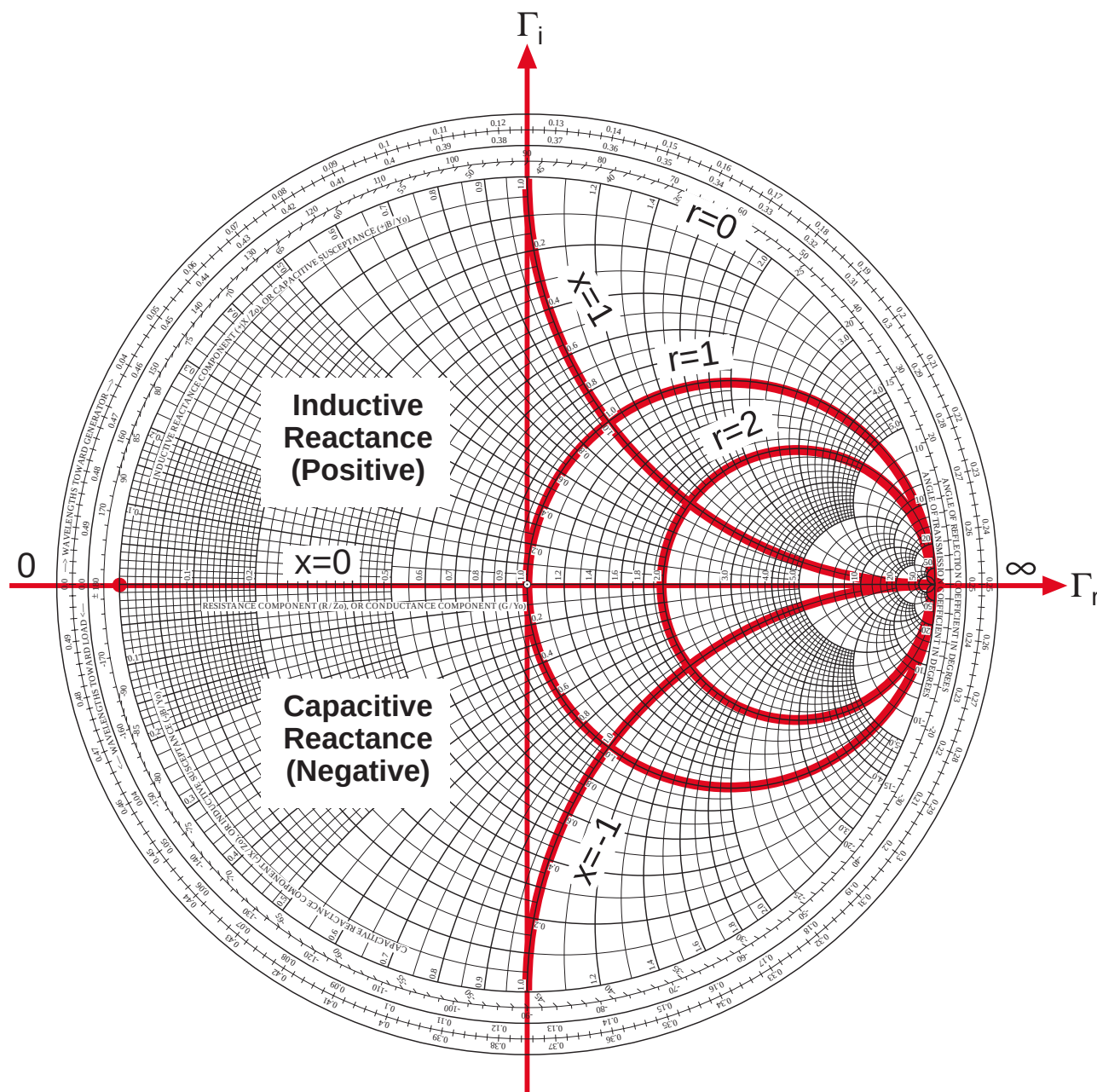
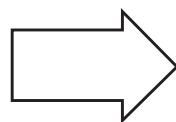
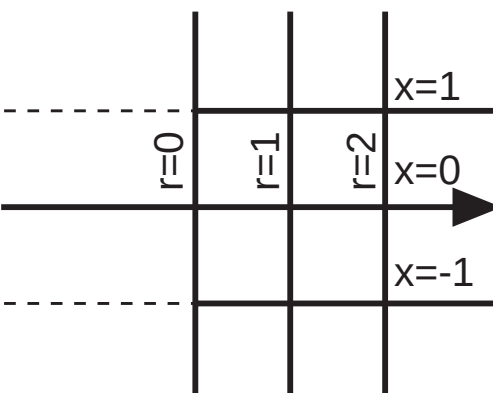
Right Half
z Plane



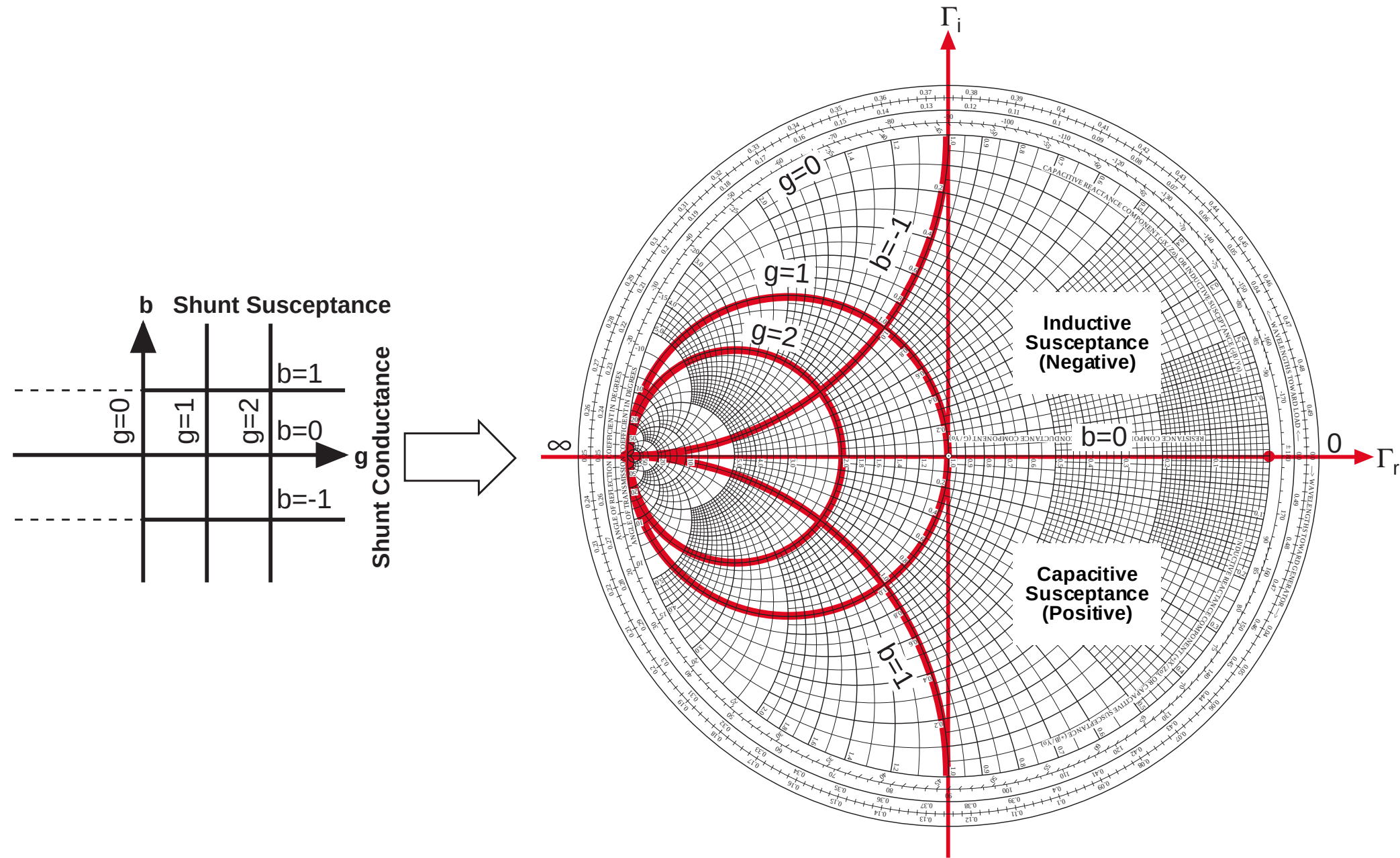
Interior Unit Circle
Γ Plane

Smith Chart: Impedance Coordinates

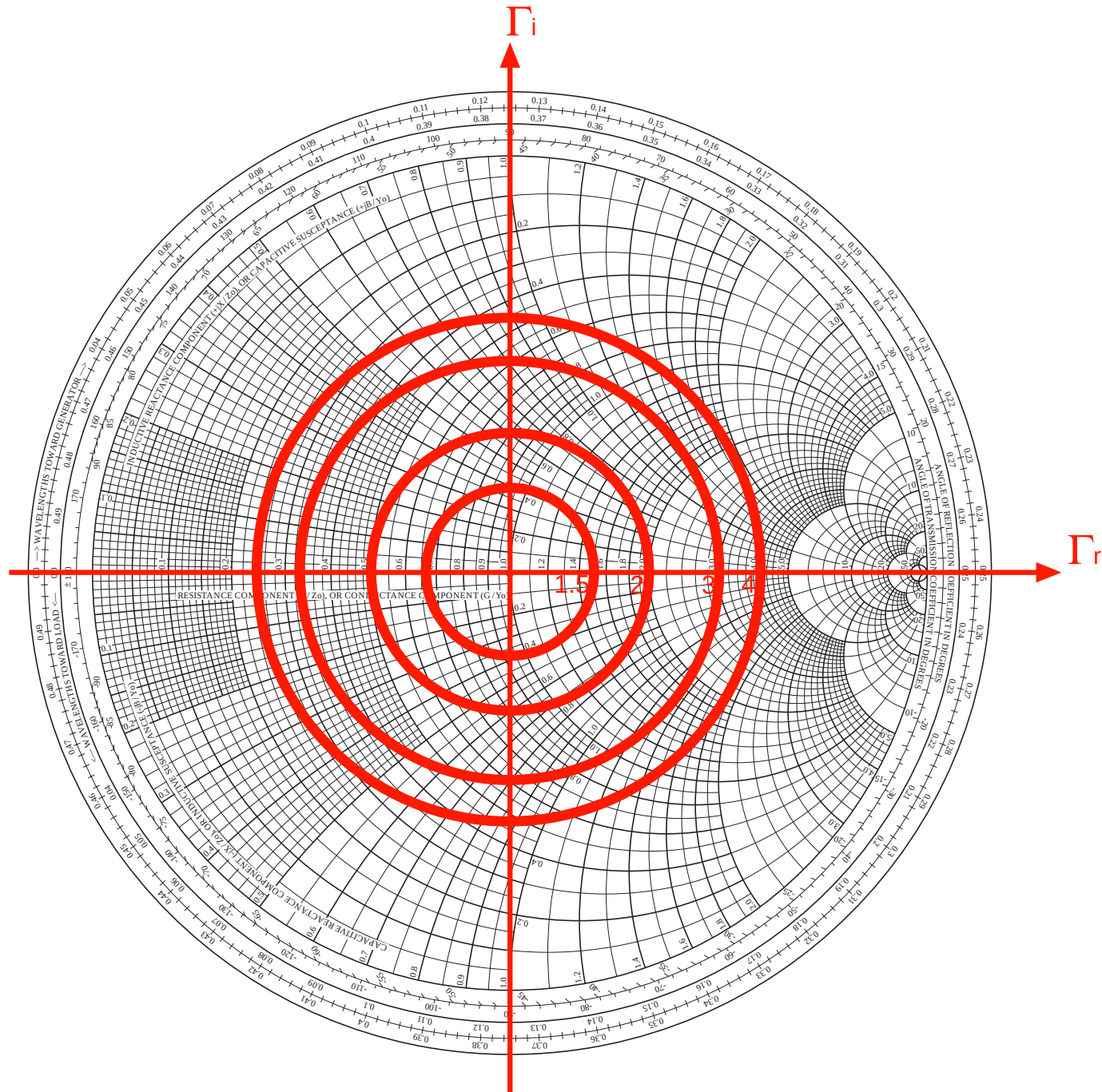
x Series Reactance



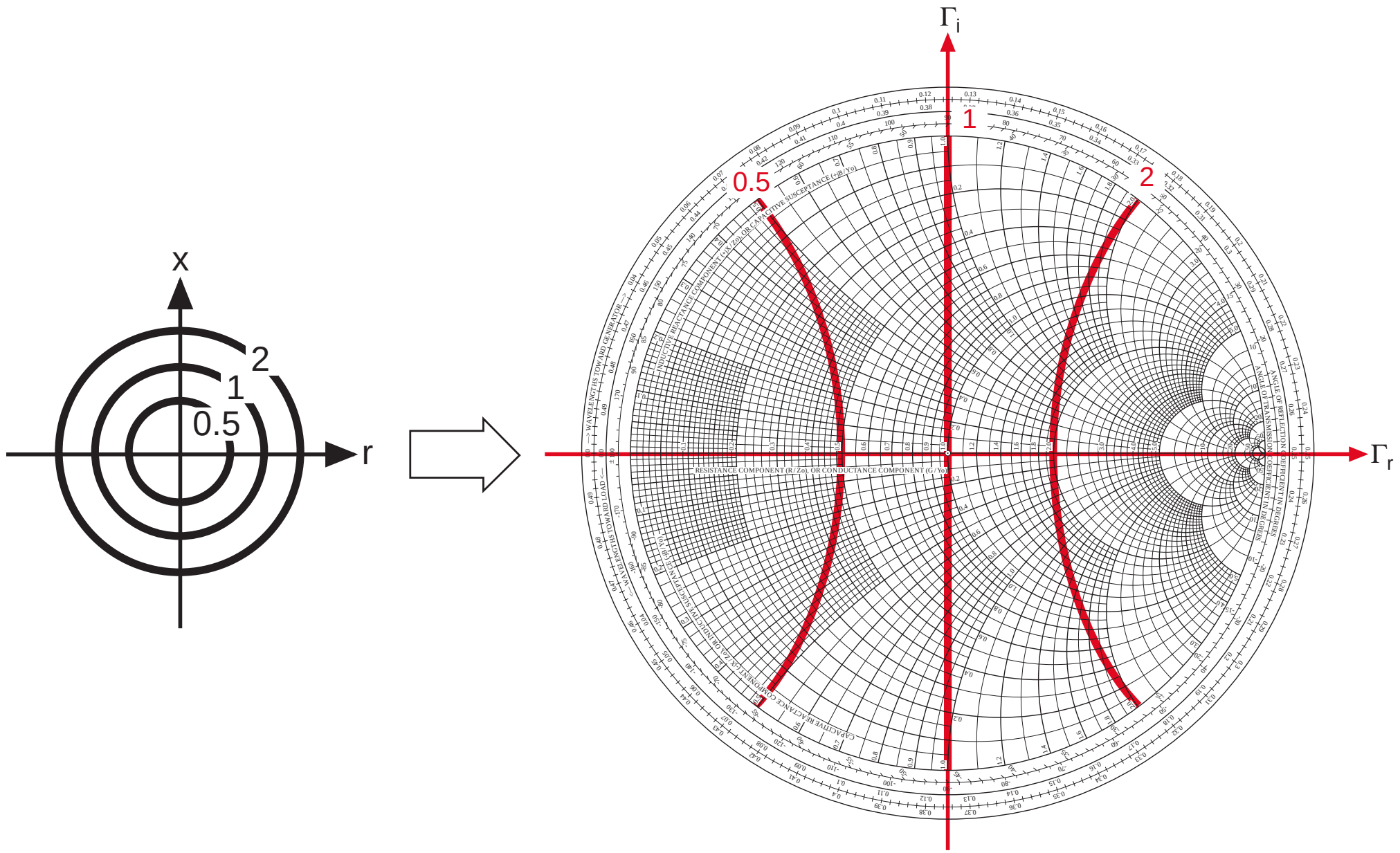
Smith Chart: Admittance Coordinates



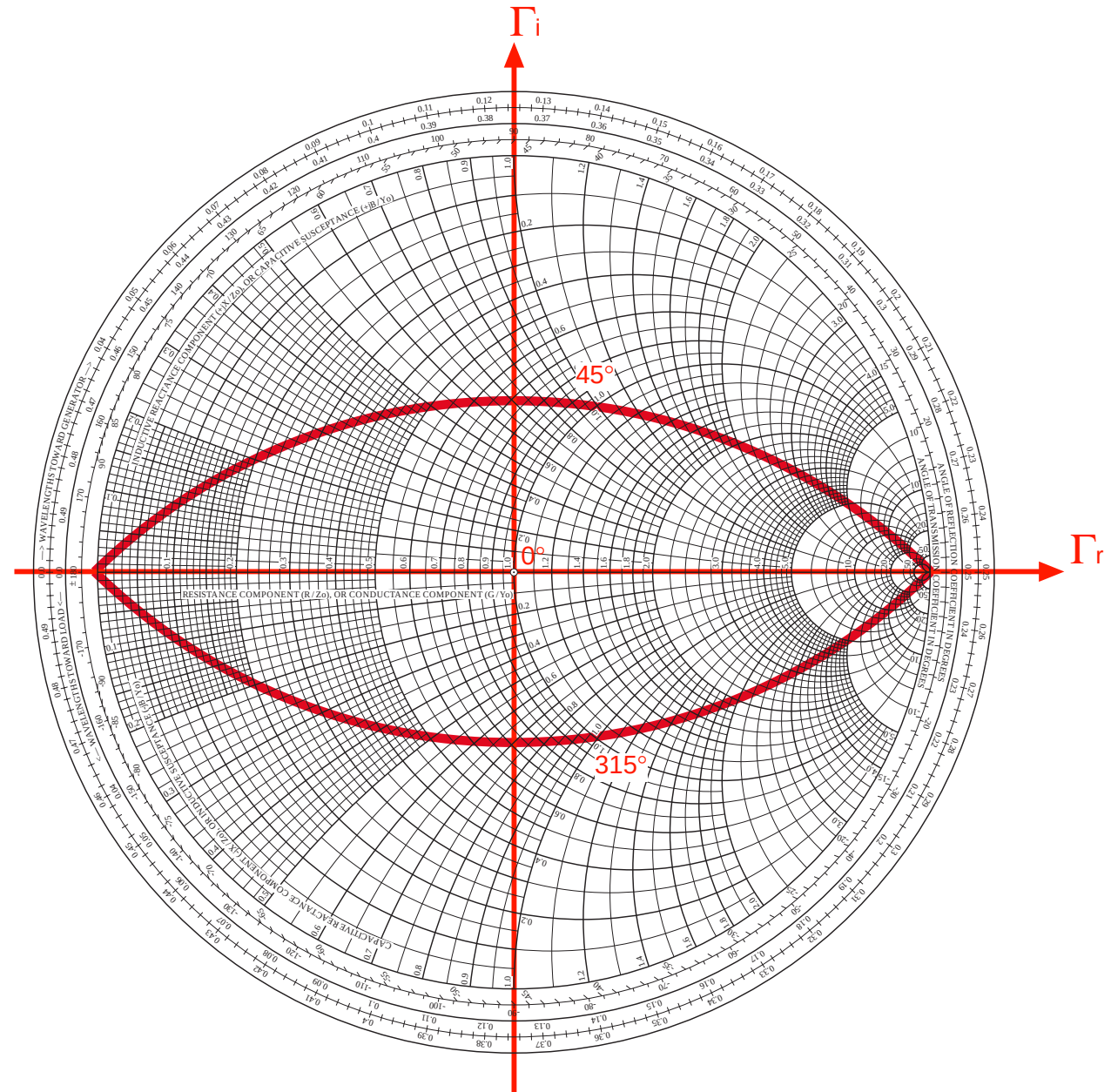
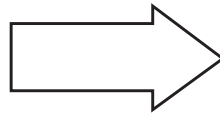
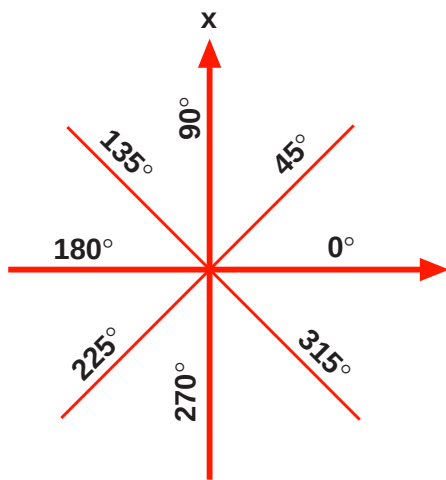
Smith Chart: Constant SWR Circles



Smith Chart: Constant Impedance Magnitude Circles **TRW**



Smith Chart: Constant Impedance Phase Angle Circles



Smith Chart: Multiplication, Division, Squares, & Square Roots



Unary Operators

squares

$$a^2$$

square roots

$$\sqrt{a}$$

tangents

$$\tan \theta$$

cotangents

$$\cot \theta$$

inverse tangents

$$\tan^{-1} a$$

Inverse cotangents

$$\cot^{-1} a$$

Binary Operators

multiplication $\times$

$$a \cdot b$$

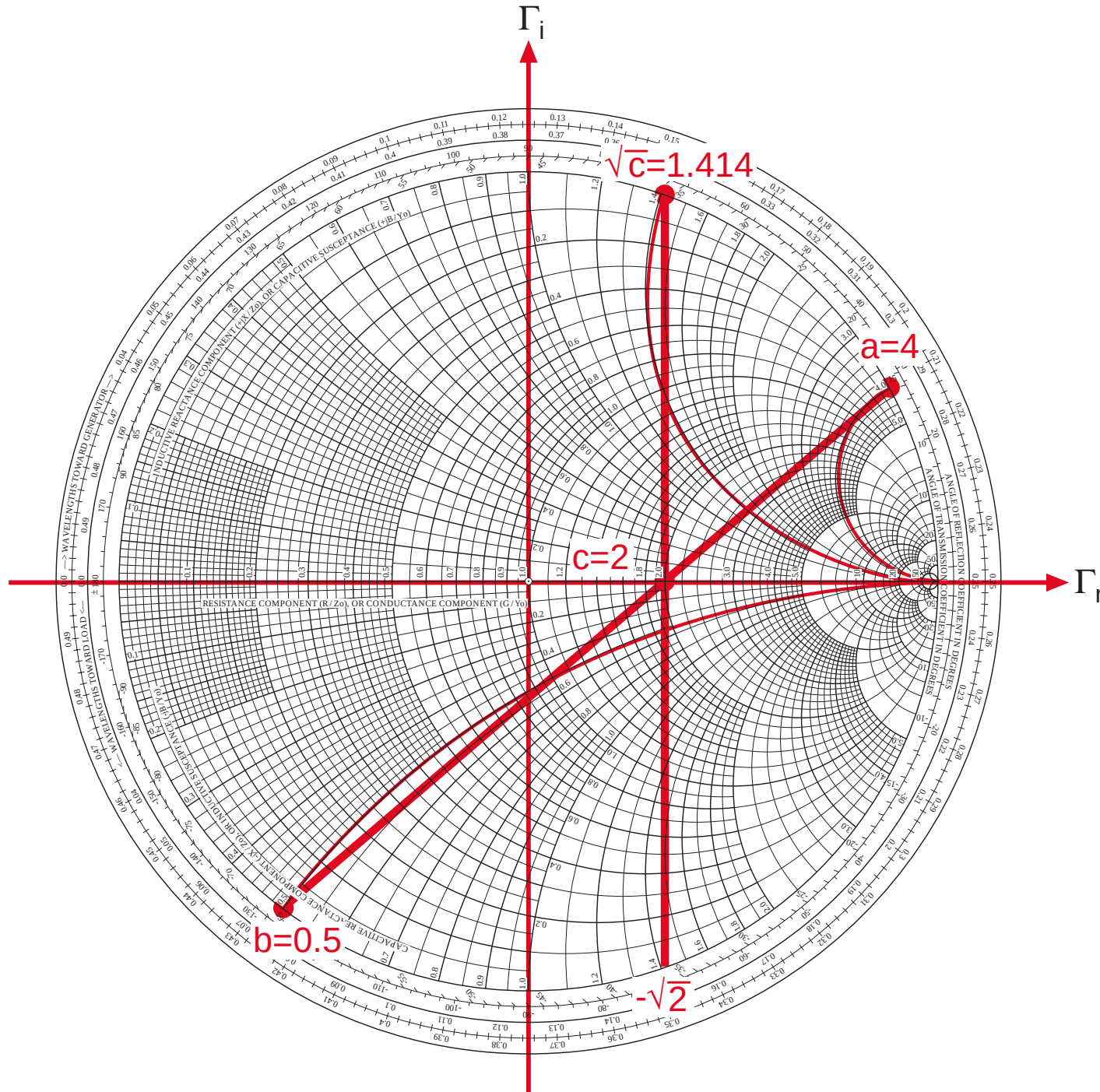
division $\div$

$$c/a$$

geometric mean

$$\sqrt{ab}$$

Smith Chart: A Nomogram for Math Calculations



Part 3: Impedance Matching

□ Single frequency matching

- Manual synthesis using Smith Chart
- Eight canonical networks
- Lumped elements
- Series and parallel stubs
- Transmission line sections

□ Multiple frequency matching

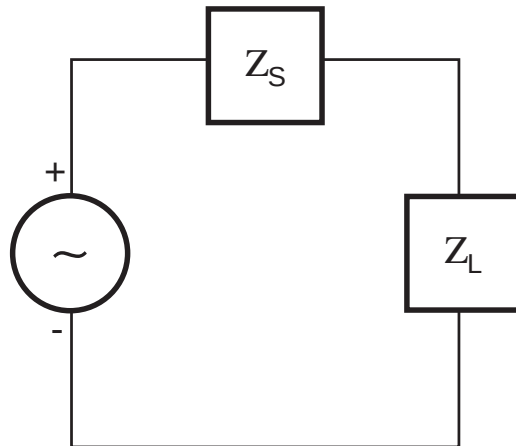
- Ladder networks
- Multiple stubs
- Multiple line sections

□ Broadband matching

- Maximize SWR bandwidth
- Numerical optimization
- winSMITH software
- Smith Chart used for visualization only

	<u>Fractional Bandwidth</u>
<i>Narrowband</i>	<i>< 10%</i>
<i>Moderate band</i>	<i>10% to 50%</i>
<i>Broadband</i>	<i>> 50%</i>

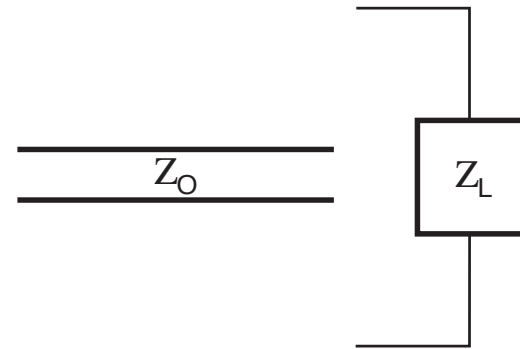
❑ *Conjugate Matching*



$$Z_S = Z_L^*$$

- ❑ *Best use at source (transmitter)*
- ❑ *Maximizes power delivery to the load*
- ❑ *Does not minimize reflections unless Z_S is real*
- ❑ *Normally done by the transmitter manufacturer at the circuit design level*
- ❑ *Ideally $Z_S(\text{ext}) = 50 \Omega$*

❑ *Load Matching*

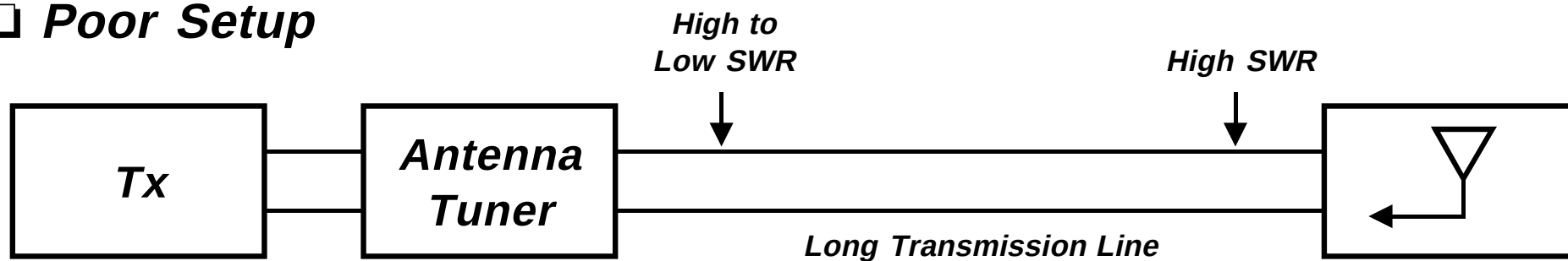


$$Z_L = Z_O$$

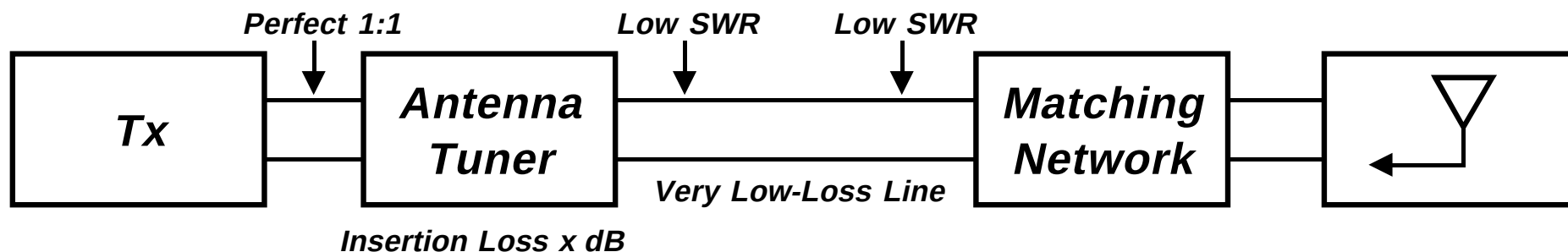
- ❑ *Best used at ends of transmission lines*
- ❑ *Minimizes reflections*
- ❑ *Does not maximize delivered power unless Z_O is real*

Where Should Matching Network Go?

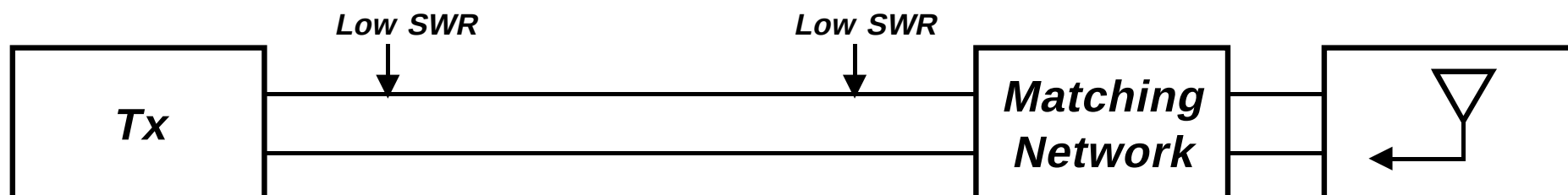
❑ Poor Setup



❑ Good Setup



❑ Best Setup



- ❑ ***Antenna analyzer***

- *Autek*
- *CIA*
- *MFJ*

- ❑ ***Noise bridge (less accurate)***

- ❑ ***Network analyzer (more accurate)***

- *Hewlett-Packard*

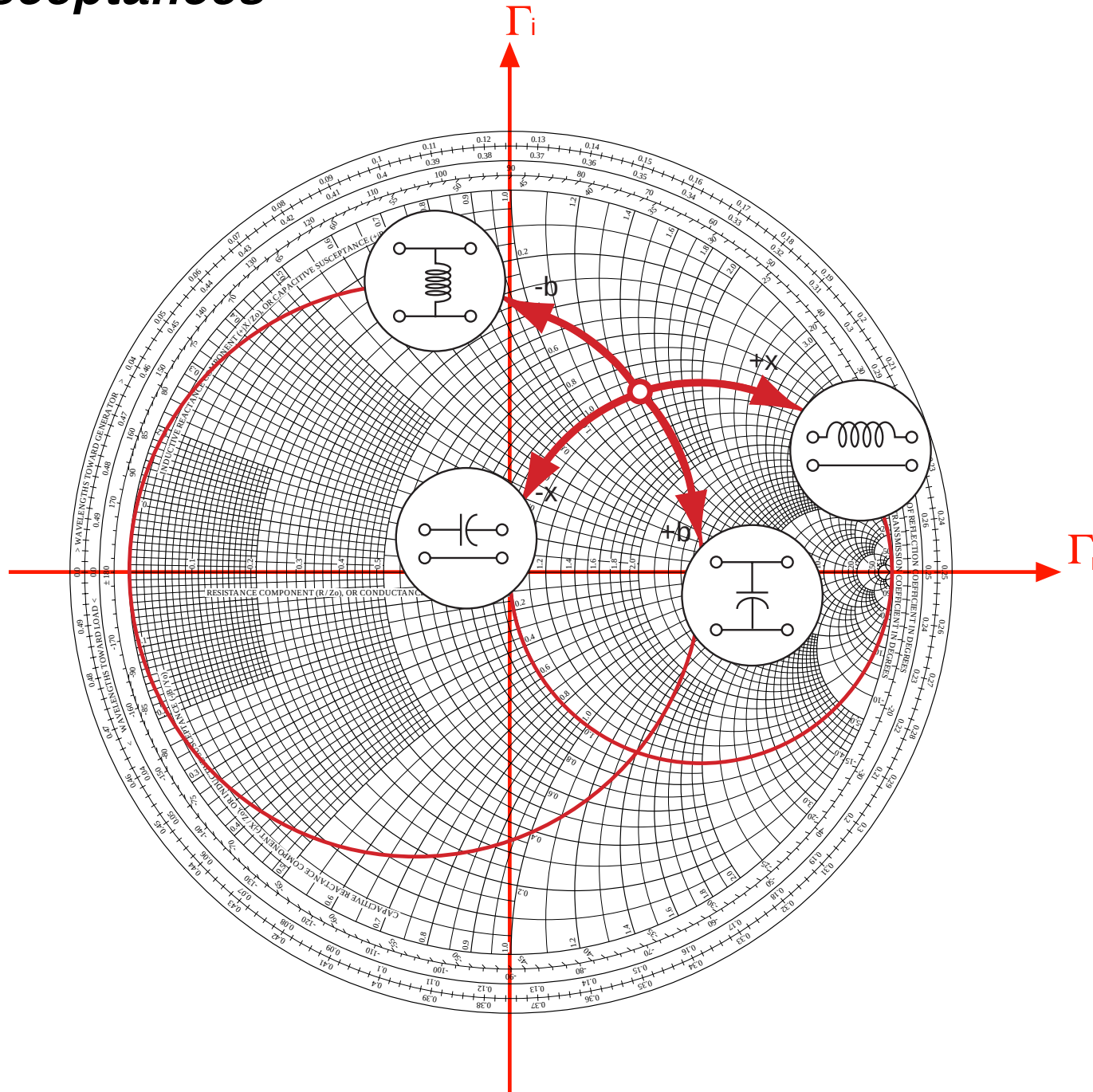
- 1. Measure transmission line parameters Z_o , v_f***
- 2. Measure antenna feedpoint impedance across band(s) of interest***
- 3. Measure or calculate impedance across band(s) of interest at network insertion point***
- 4. Narrowband match:***
 - *Select appropriate lossless L network, 2 or 4 choices*
 - *Select lumped elements vs stubs*
 - *Calculate component values*
 - *Calculate SWR and SWR bandwidth*
 - *Build and test*
- 5. Broadband match:***
 - *Use design software - winSMITH or equivalent*
 - *Design n-stage lossless ladder network*
 - *Select lumped elements vs stubs*
 - *Calculate component values*
 - *Calculate SWR and SWR bandwidth*

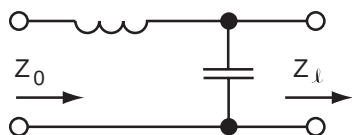
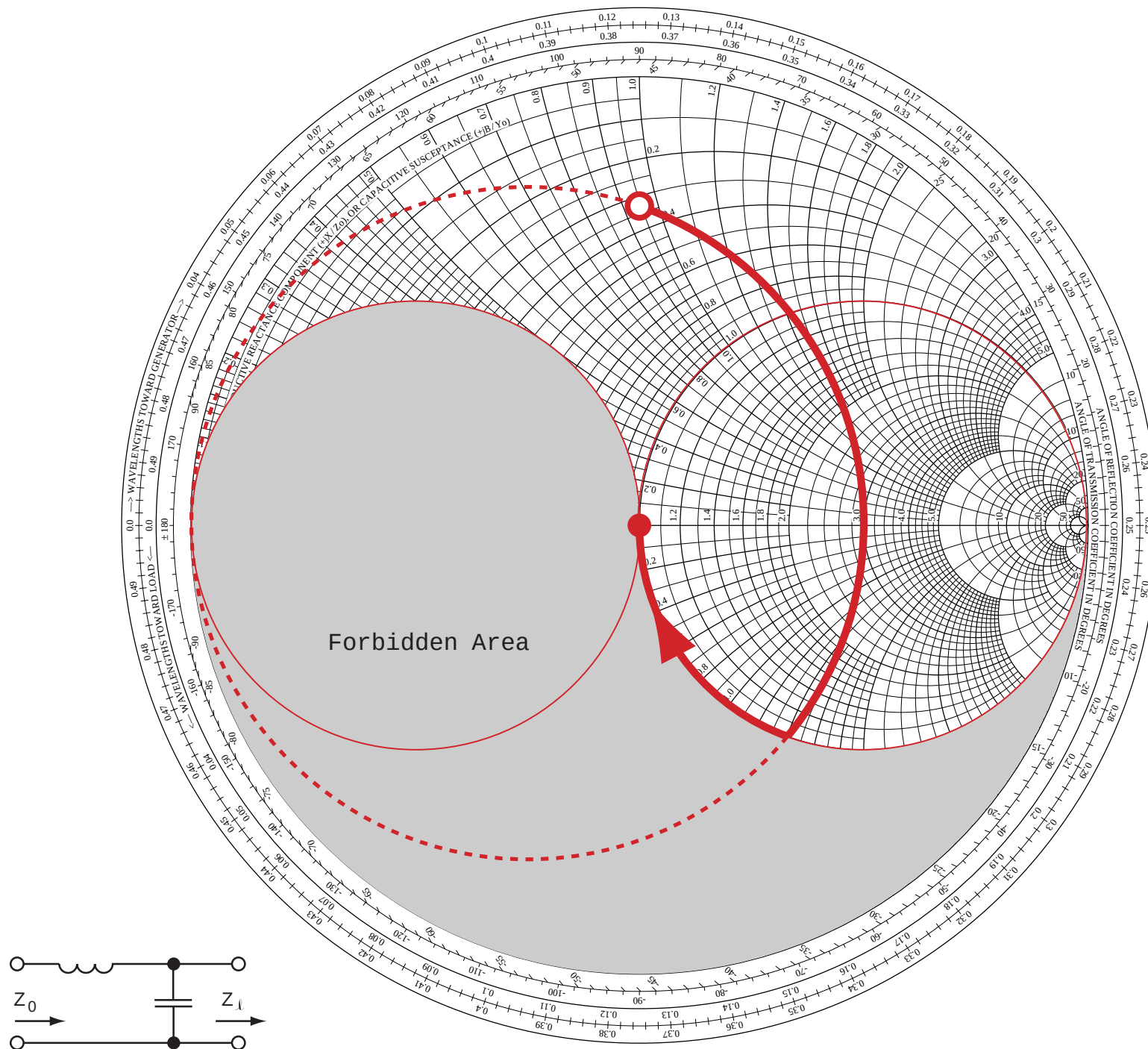
How to Measure Antenna Feedpoint Impedance

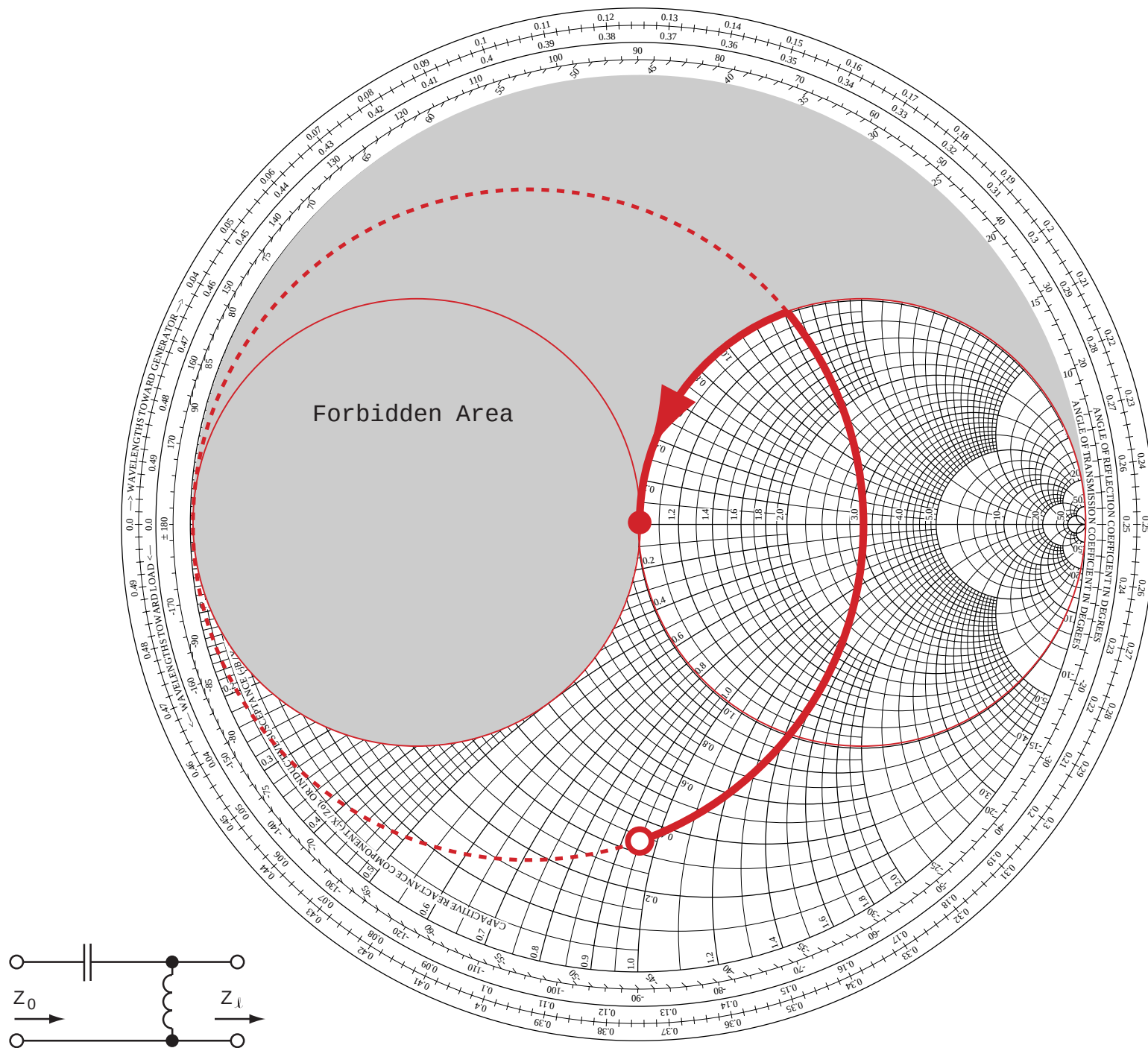


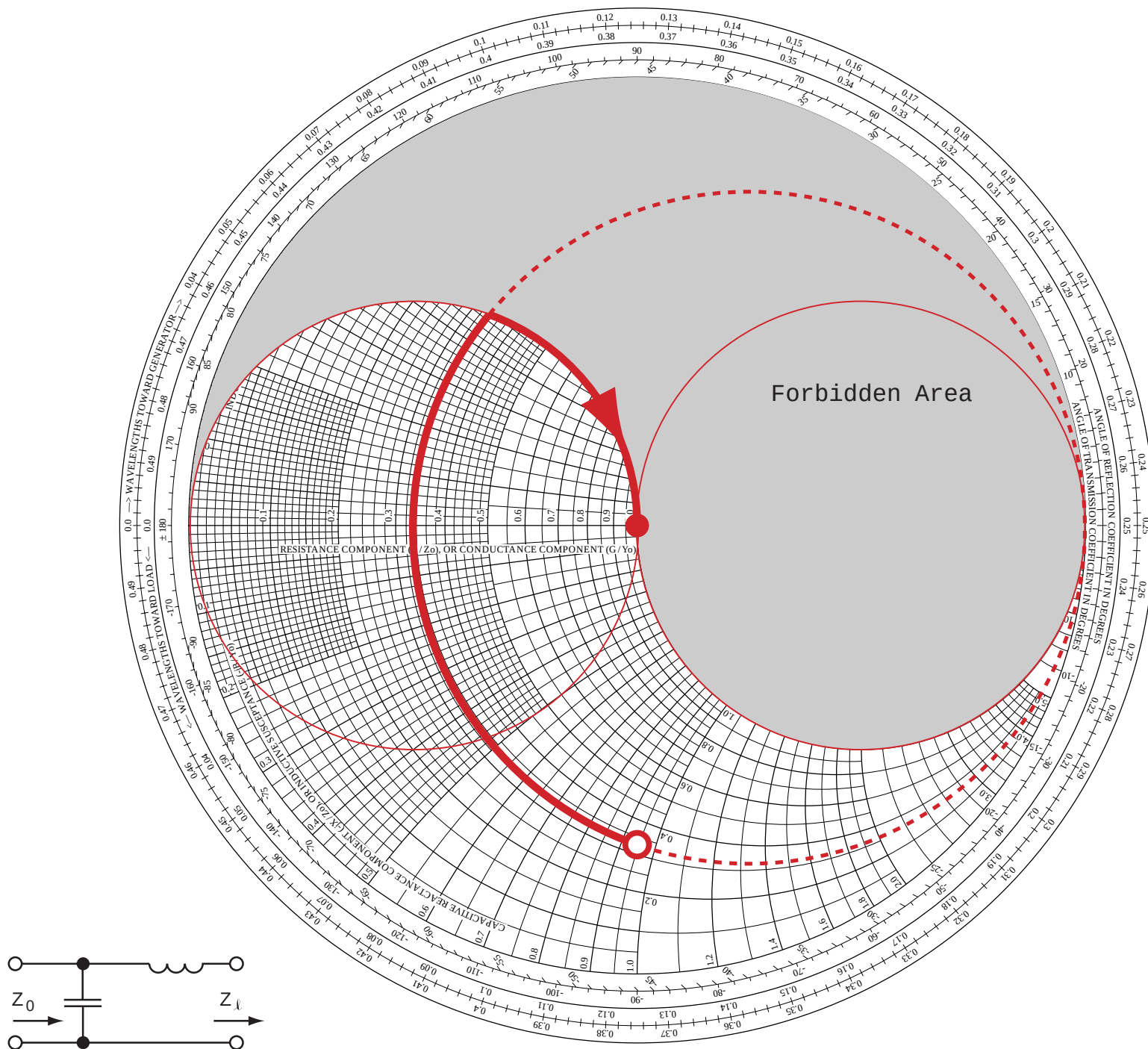
- ☐ ***Measure impedance through known line***
- ☐ ***Divide measure impedance by Z_o***
- ☐ ***Plot impedance point on Smith Chart***
- ☐ ***Move counter clockwise on chart by electrical length of line***
- ☐ ***Read coordinate values from chart***
- ☐ ***Multiply result by Z_o***

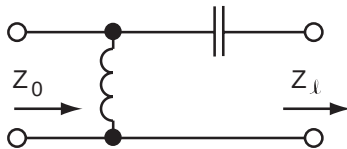
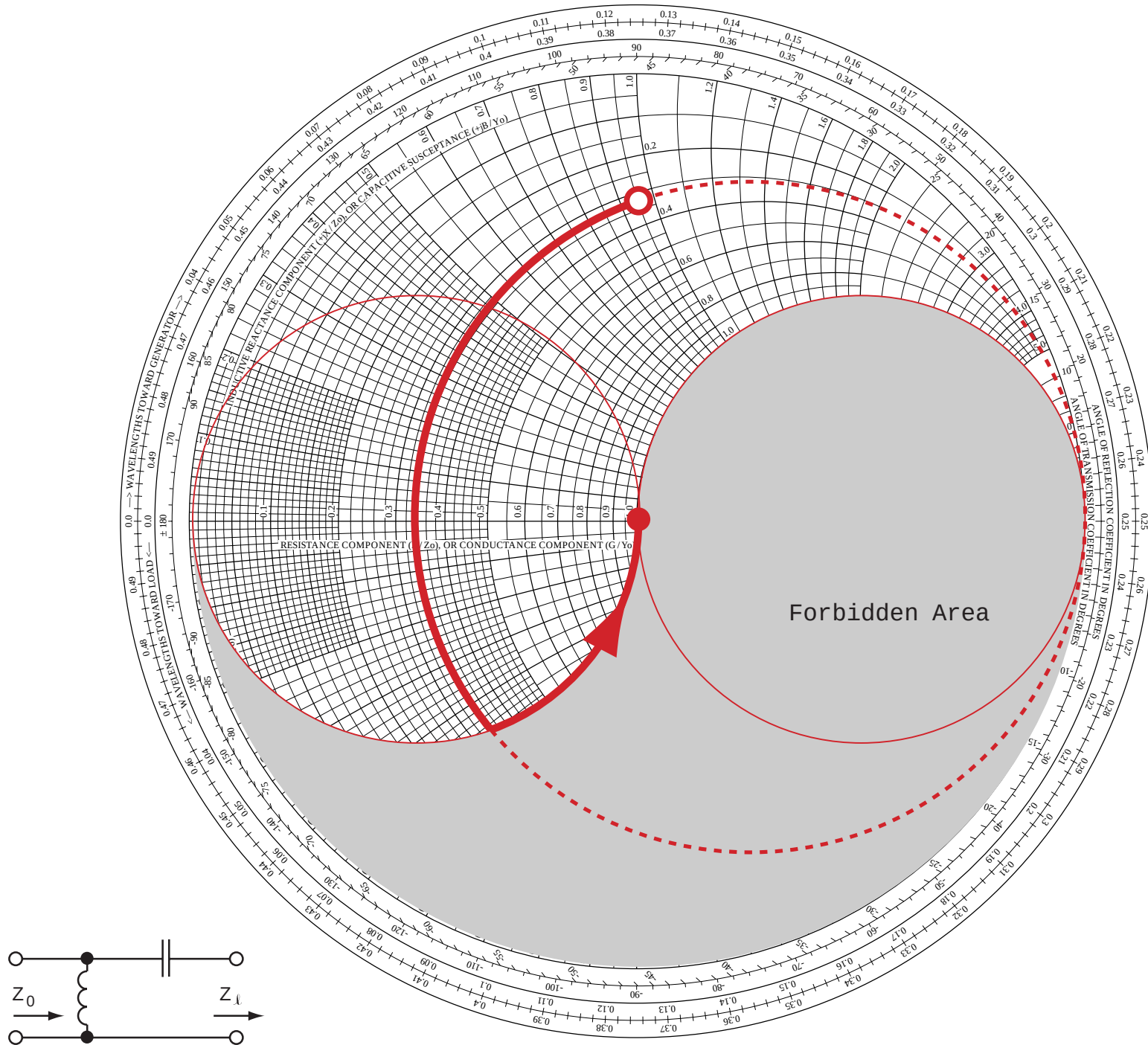
Smith Chart: Effect of Adding Series Reactances or Shunt Susceptances



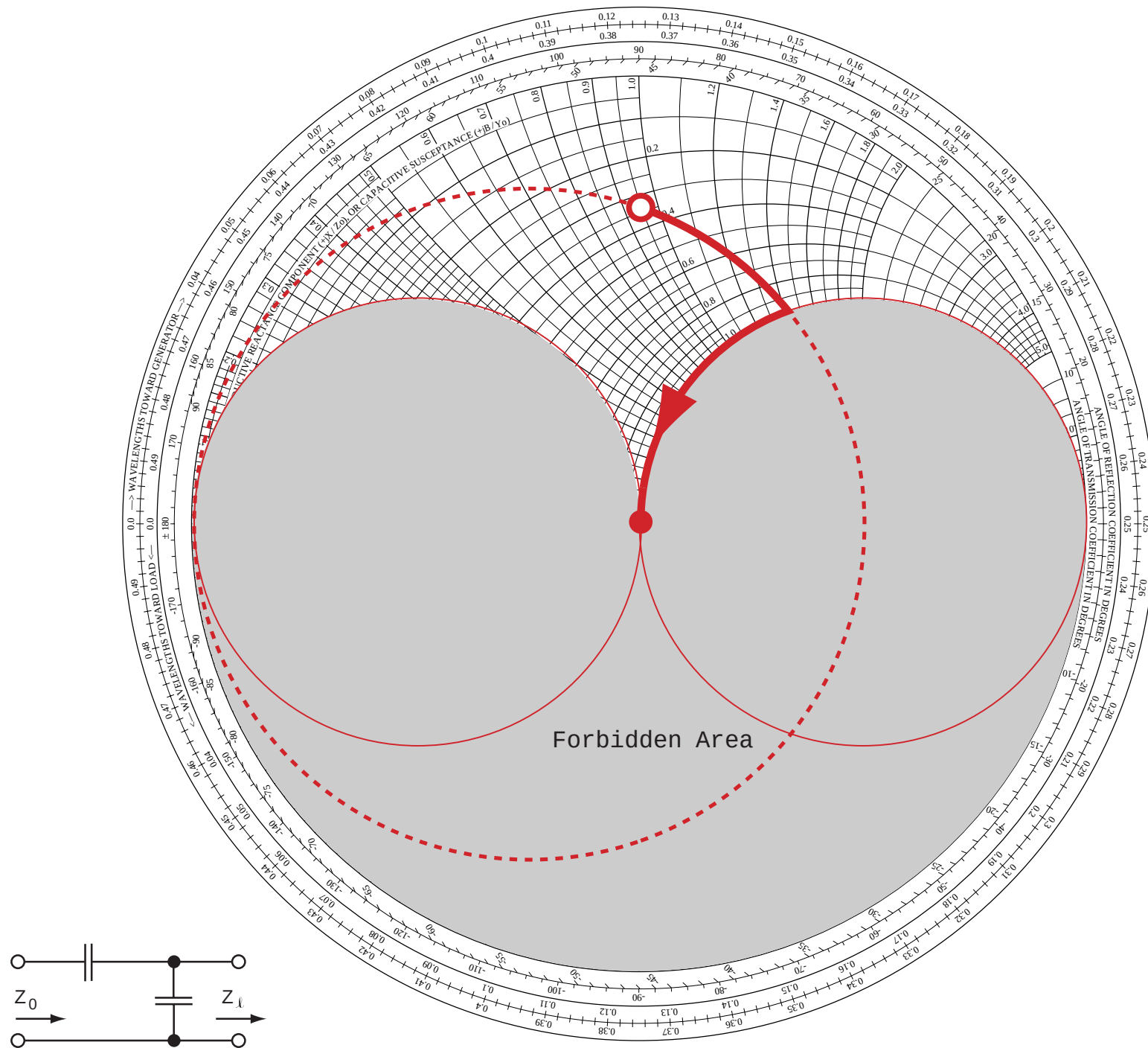




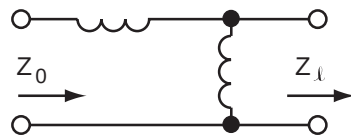
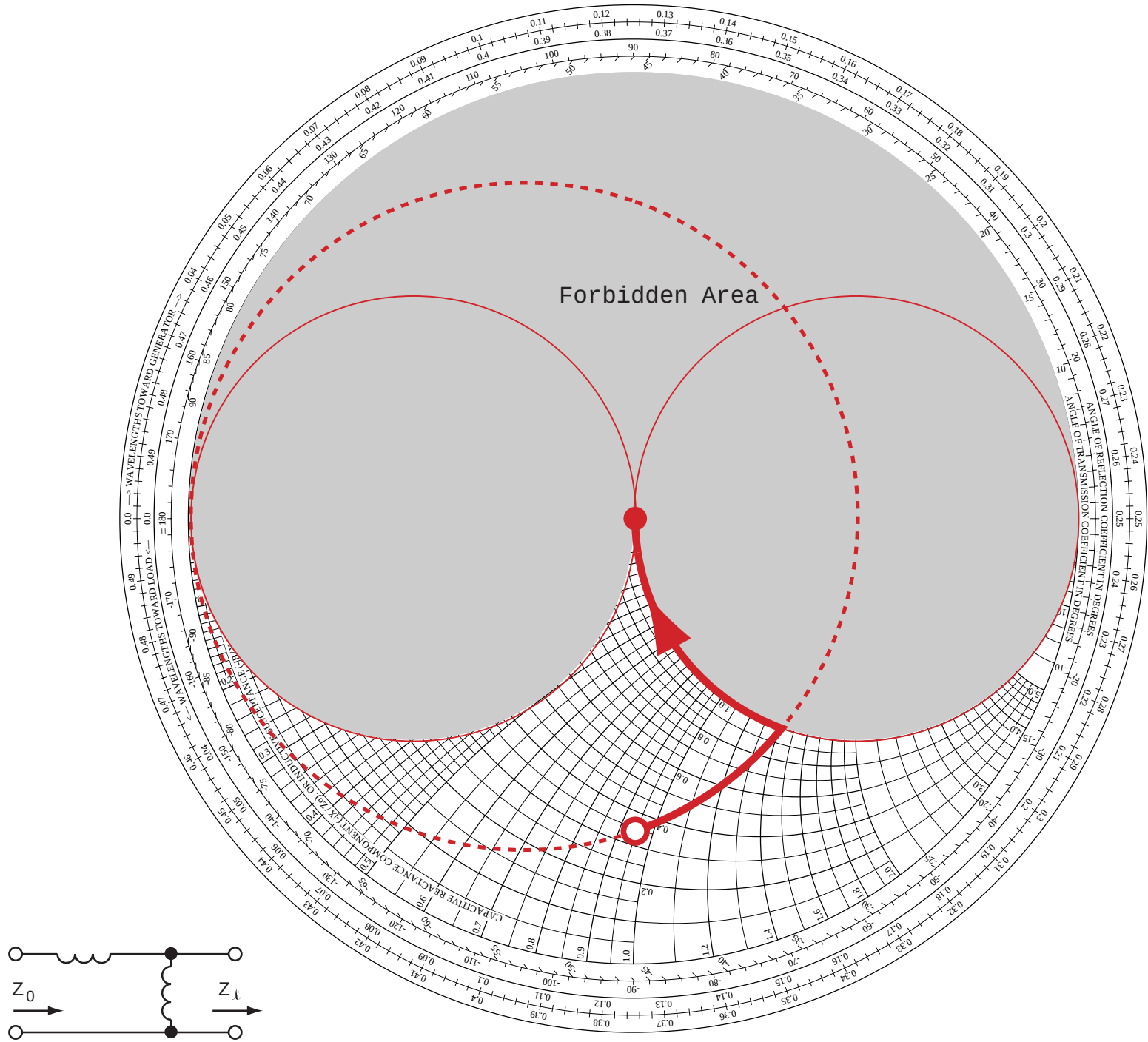




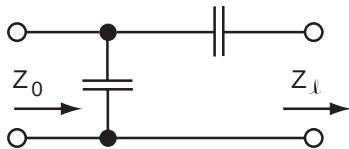
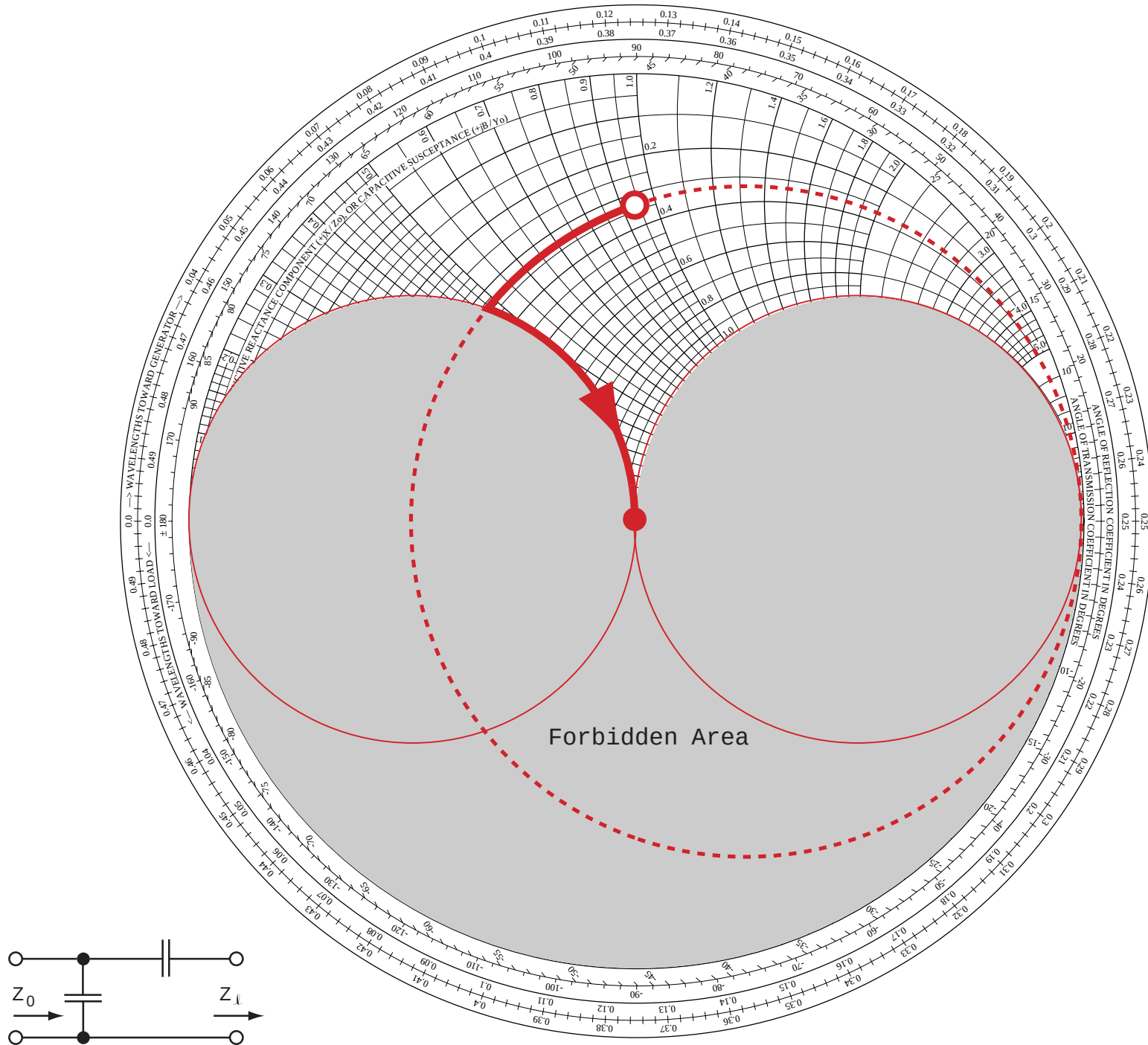
(d)



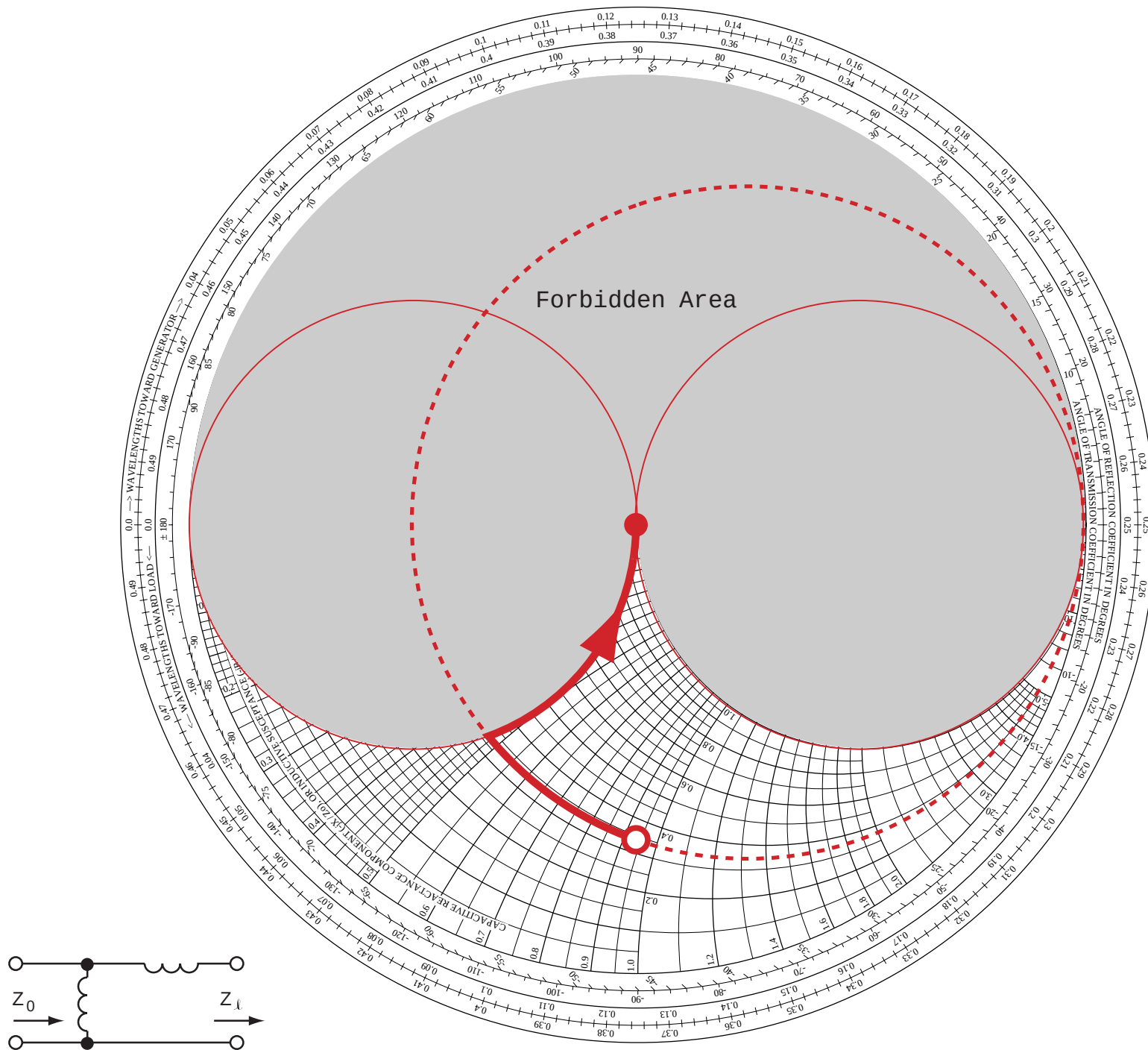
(e)



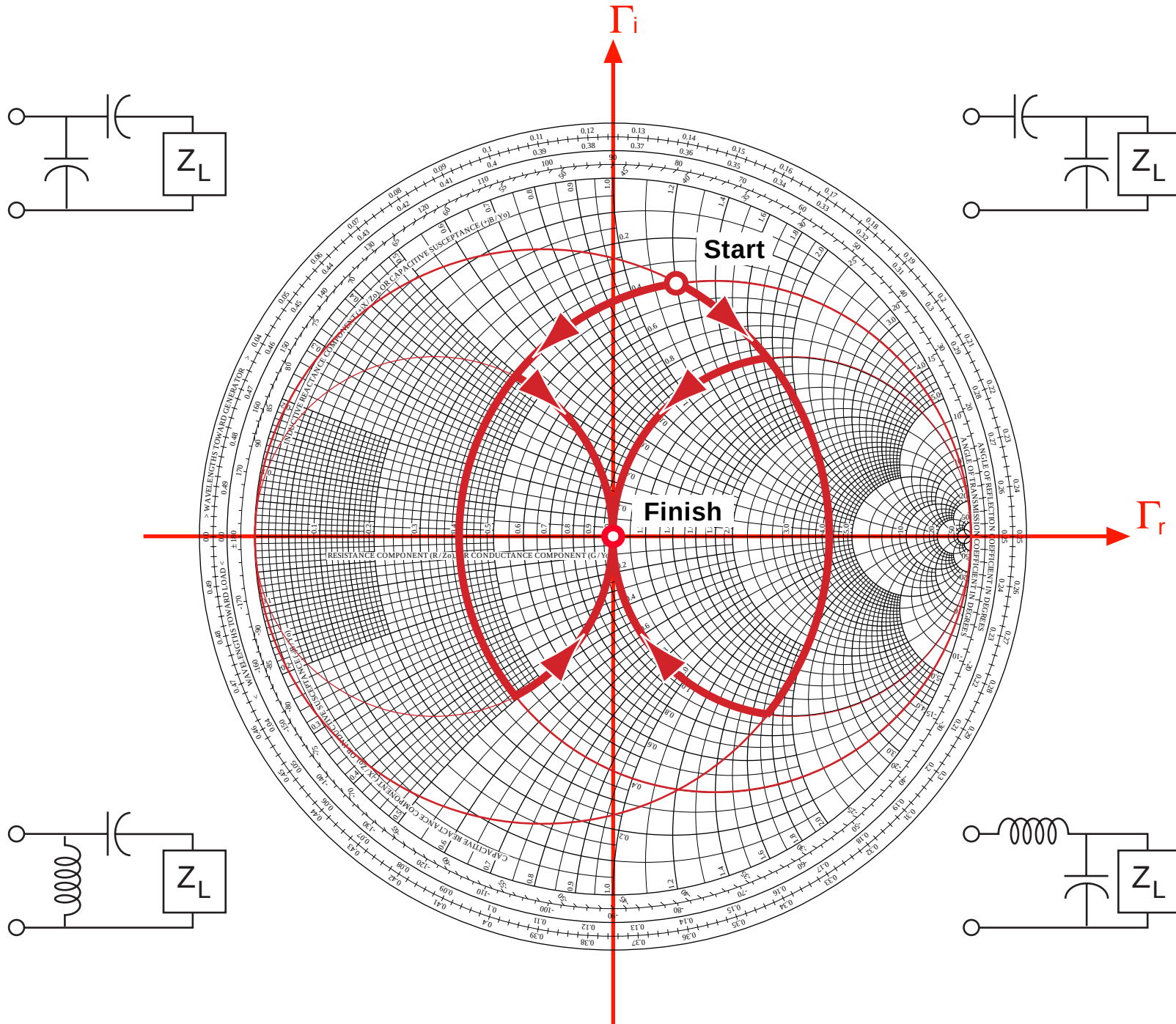
(f)



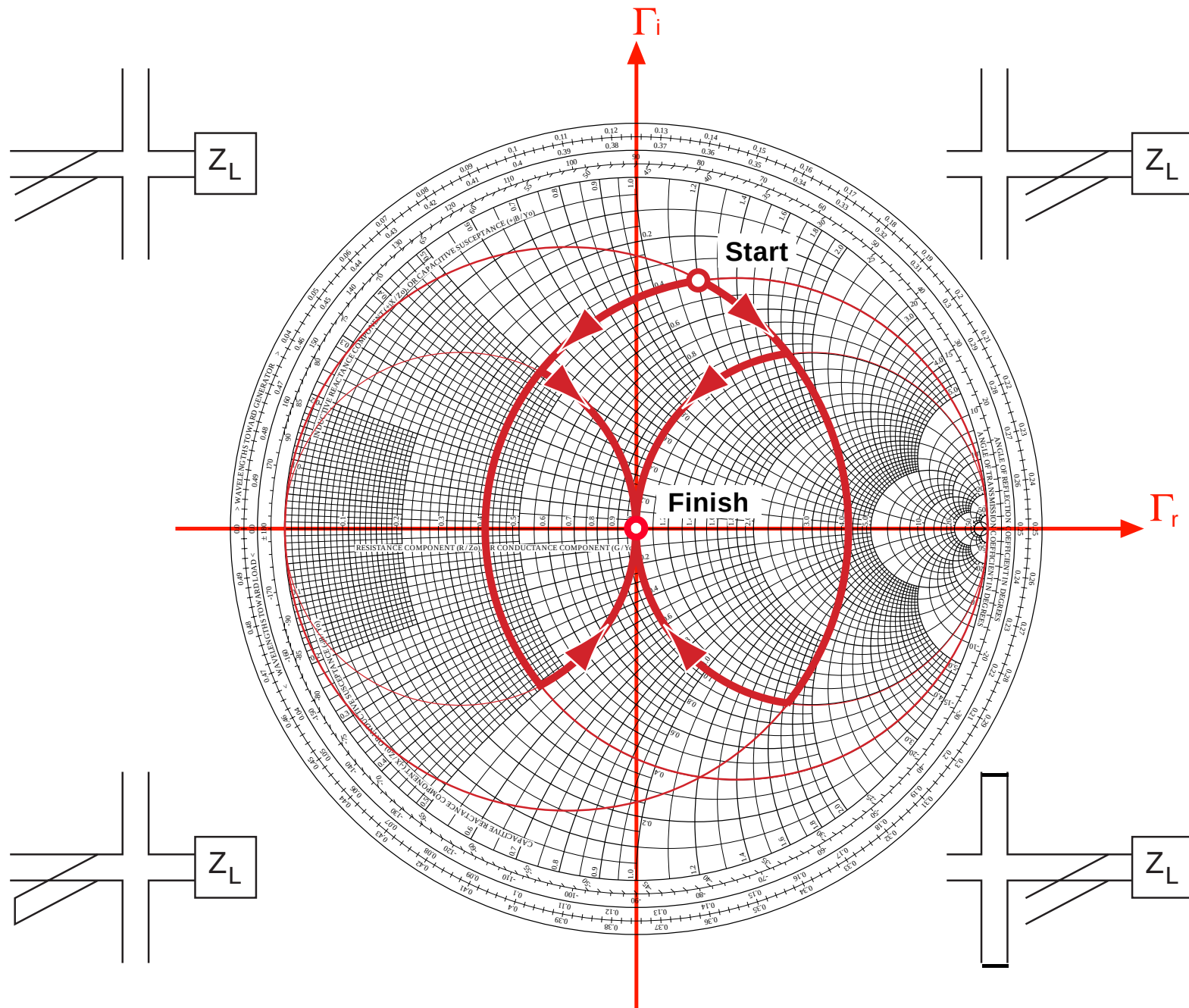
(g)



Matching: Four L-Networks Using Lumped Elements



Matching: Four L-Networks Using Stubs



Inductors

$$X_L = 2\pi fL$$

$$B_L = \frac{-1}{2\pi fL}$$

Capacitors

$$X_C = \frac{-1}{2\pi fC}$$

$$B_C = 2\pi fC$$

□ Assuming Z_o is real, then

□ Shorted Stubs 

$$X_{\text{shorted}} = Z_o \tan\left(\frac{2\pi l f}{v_f c}\right)$$

$$B_{\text{shorted}} = \frac{-1}{Z_o \tan\left(\frac{2\pi l f}{v_f c}\right)}$$

□ Open Stubs 

$$X_{\text{open}} = \frac{-Z_o}{\tan\left(\frac{2\pi l f}{v_f c}\right)}$$

$$B_{\text{open}} = \frac{1}{Z_o} \tan\left(\frac{2\pi l f}{v_f c}\right)$$

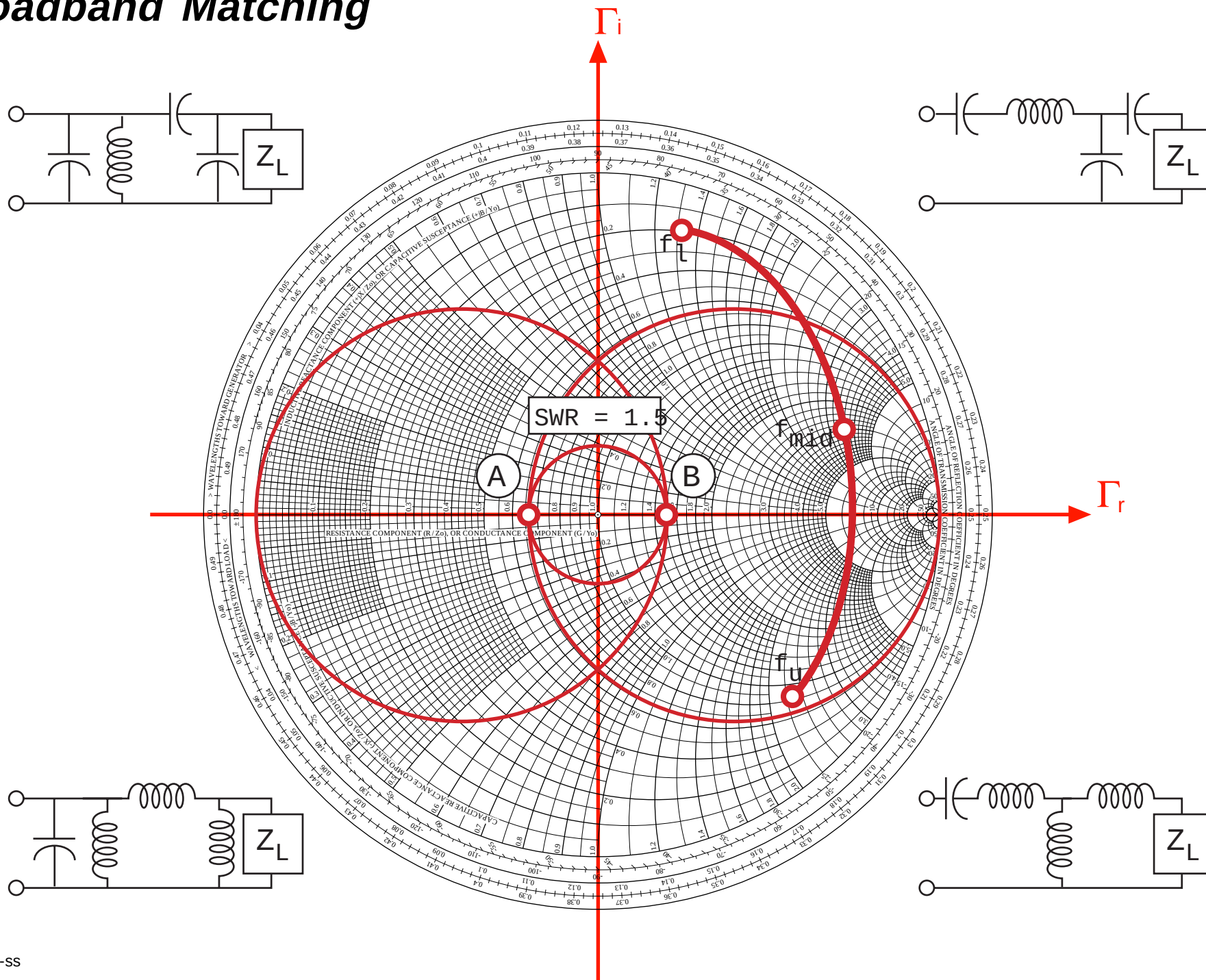
Broadband Matching Network Design Recipe

Using 4-Element/ π -Resonant and T-Resonant Networks

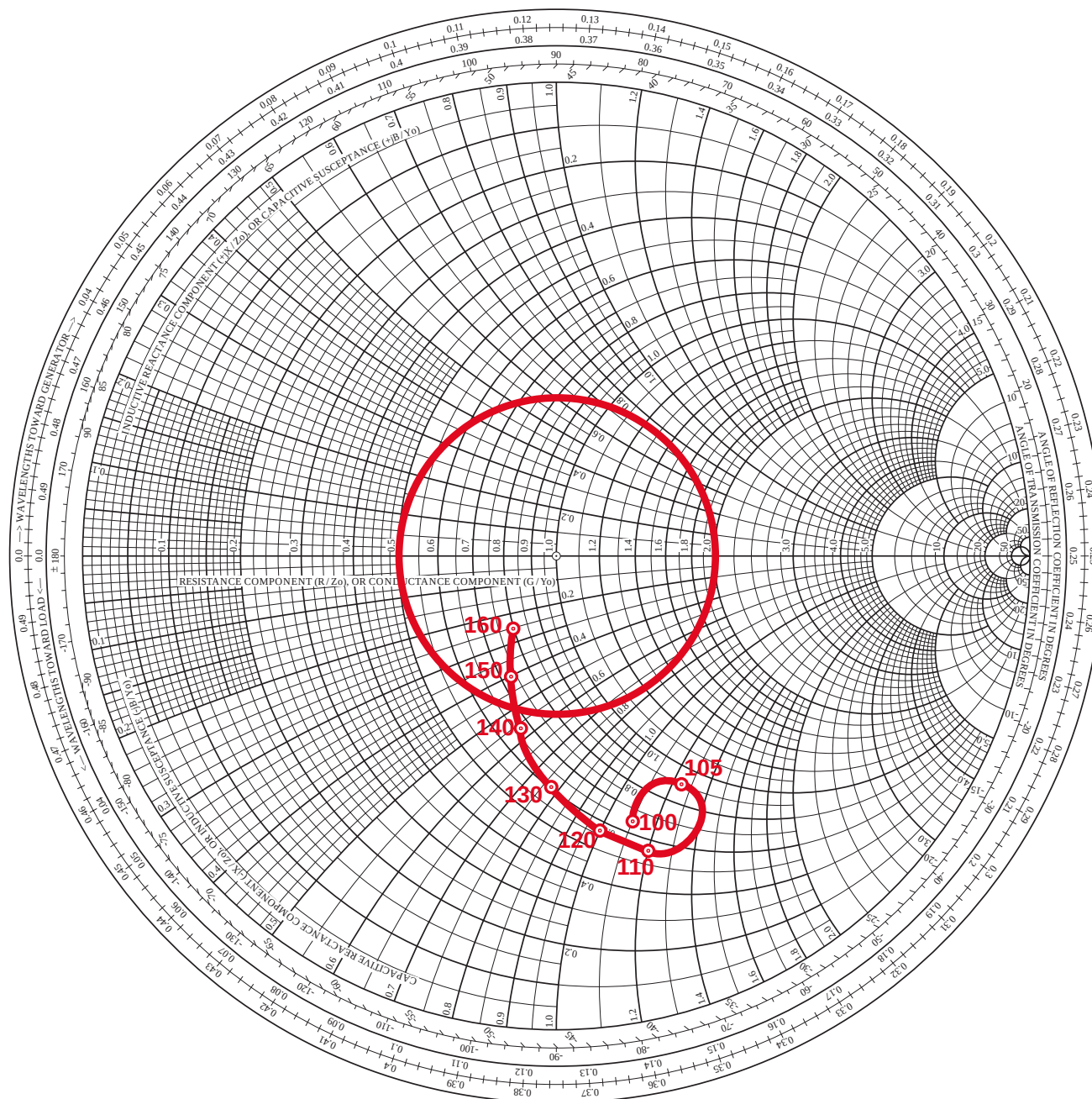


- Putting network insertion point close to load (antenna) gives greatest SWR bandwidth***
- Step 1: Using an L-network, move the midband impedance point to prime point A or B. Bandwidth will be maximized if the minimum reactance or susceptance L-network is chosen in this step.***
- Step 2: Wrap the impedance locus into the SWR circle by adding a series or parallel resonant circuit as required to complete the π -resonant or T-resonant network***

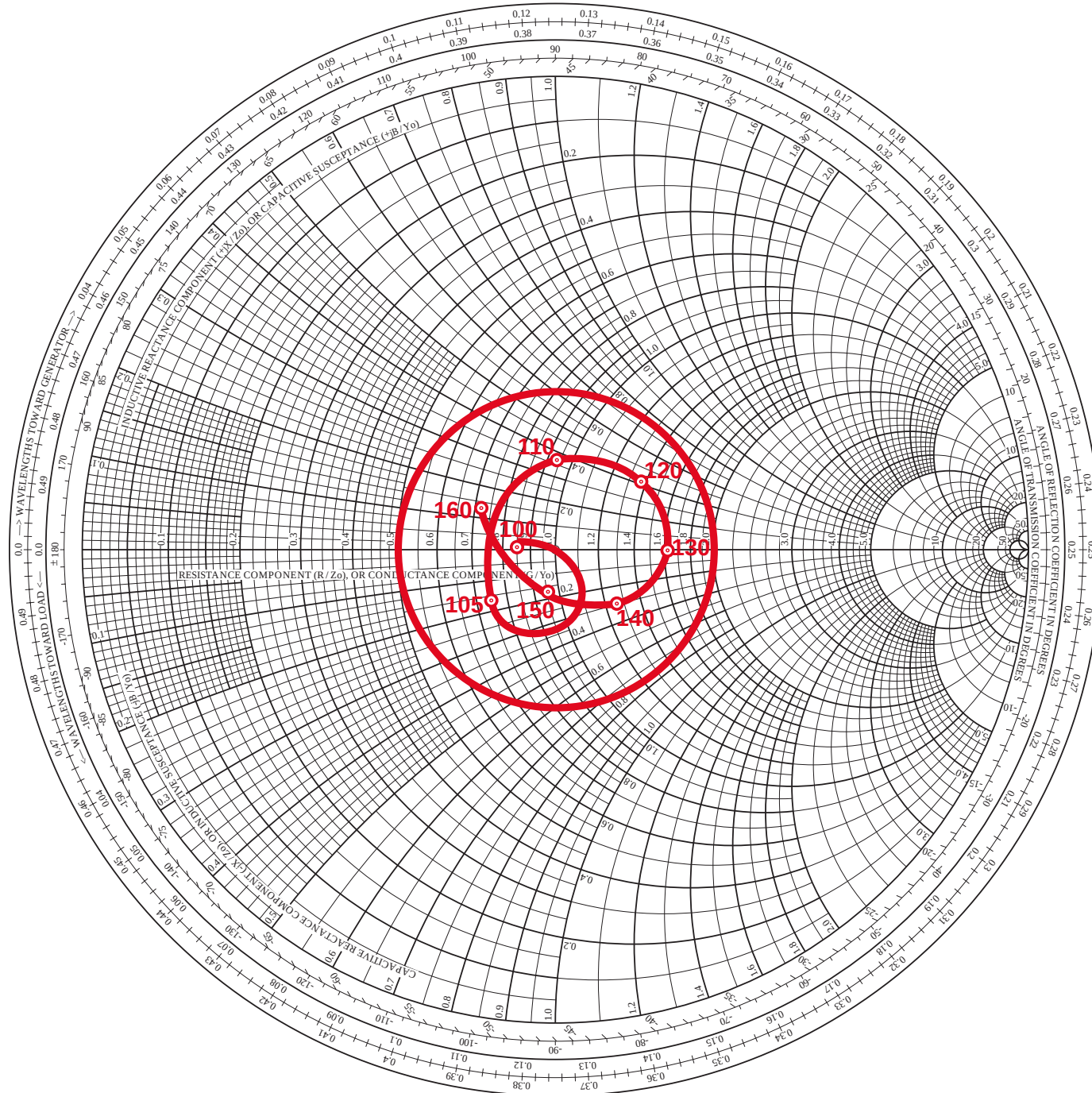
Π - Resonant and T-Resonant Moderate and Broadband Matching



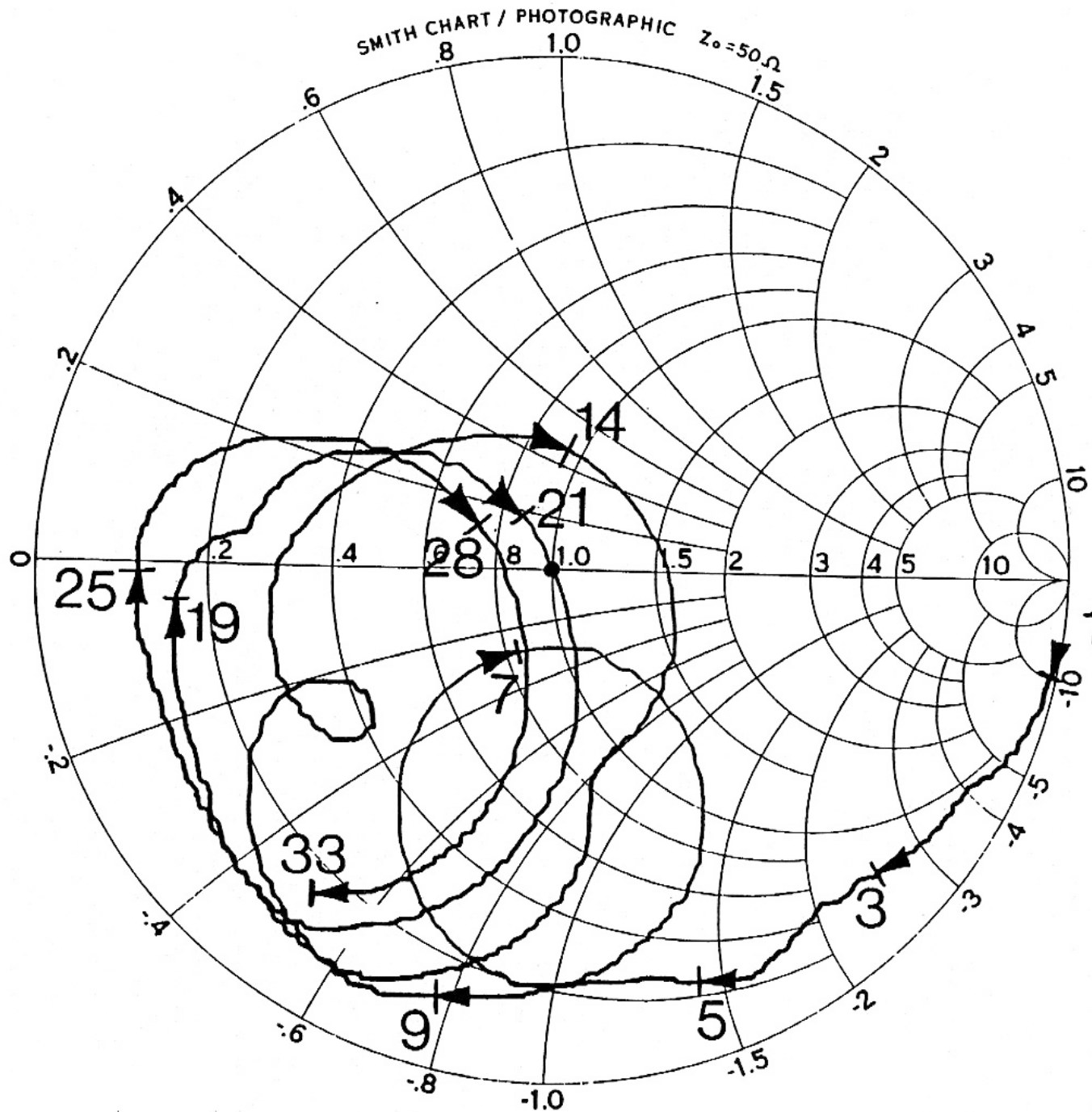
Example A: Moderate Band Matching Problem



Example A: Results of Narrowband Matching



Example B: Multiple Frequency Antenna



Smith Chart Analysis & Display

MicroSmith 2.3, ARRL, 1992, \$39

winSMITH 2.0, Noble Publishing, 1995, \$79

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